

# PERIODIC INFLOW DESIGN FLOOD CONTROL SYSTEM PLAN

EXISTING CCR IMPOUNDMENTS  
*CCR Rule Section 257.82*

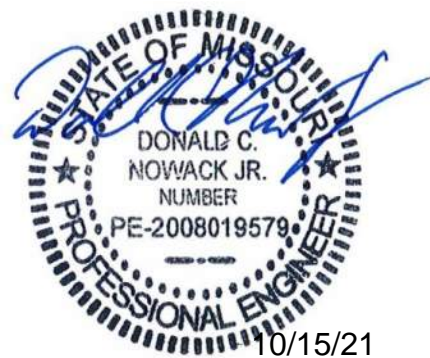
## ASBURY POWER PLANT

21133 Uphill Lane  
Asbury, Missouri 64832

October 15, 2021

**The Empire District Electric Company**

Prepared by:



Donald C. Nowack, P.E., R.G.  
MO P.E. 2008019579  
MO R.G. 2001011344

October 15, 2021

The Empire District Electric Company  
Asbury Power Plant  
21133 Uphill Lane  
Asbury, Missouri 64832

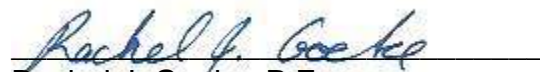
RE: **Periodic Inflow Design Flood Control System Plan –**  
CCR Rule Section 257.82  
The Empire District Electric Company – Asbury Power Plant  
Asbury, Missouri  
PPI Project Number 231518

To Whom It May Concern:

This document presents the **Periodic Inflow Design Flood Control System Plan** for The Empire District Electric Company's CCR Impoundment at the Asbury Power Plant. This document has been prepared to meet the requirements of Section 257.82 of the CCR Rule.

In accordance with Section 257.105(g)(4), a copy of this document should be placed in The Empire District Electric Company's operating record. In accordance with Section 257.107(g)(4), this document should also be posted to The Empire District Electric Company's CCR Compliance website. Notification of the availability of this document should be provided to the State Director, as required in Section 257.106(g)(4).

PALMERTON & PARRISH, INC.  
By:



Rachel J. Goeke, P.E.  
MO P.E. 2007020268

PALMERTON & PARRISH, INC.  
By:



Donald C. Nowack, P.E., R.G.  
MO P.E. 2008019579  
MO R.G. 2001011344

## TABLE OF CONTENTS

1.0	INTRODUCTION .....	1
2.0	ANALYSIS OF EXISTING INFLOW DESIGN FLOOD CONTROL SYSTEM .....	1
2.1	Hazard Classification and Design Assumptions .....	1
2.2	Hydrologic and Hydraulic Model.....	2
2.3	Hydrologic and Hydraulic Modeling Results .....	5
2.4	Conclusions.....	5
3.0	INFLOW DESIGN FLOOD CONTROL SYSTEM PLAN .....	6
3.1	Contingency Planning .....	7
4.0	CCR RULE SECTION 257.82(c)(5) – CERTIFICATION .....	7

## APPENDICES

APPENDIX I	–	FIGURES
APPENDIX II	–	PRECIPITATION TABLE & PIPE FLOW CALCULATIONS
APPENDIX III	–	HEC OUTPUT

FIGURE 1	–	SITE LOCATION ON TOPOGRAPHIC MAP
FIGURE 2	–	SITE LOCATION ON 2013 AERIAL PHOTOGRAPH
FIGURE 3	–	ASBURY CCR IMPOUNDMENT

# **PERIODIC INFLOW DESIGN FLOOD CONTROL SYSTEM PLAN – EXISTING CCR IMPOUNDMENTS**

## **CCR RULE SECTION 257.82**

### **THE EMPIRE DISTRICT ELECTRIC COMPANY – ASBURY POWER PLANT**

#### **ASBURY, MISSOURI**

## **1.0 INTRODUCTION**

This Periodic Inflow Design Flood Control System Plan has been prepared according to the U. S. Environmental Protection Agency final rule regarding the disposal of coal combustion residuals from electric utilities (40 CFR Part 257 and 261, also known as the CCR Rule). The CCR Rule Section 257.82 requires the owner or operator of an existing or new CCR surface impoundment or any lateral expansion of a CCR surface impoundment must design, construct, operate, and maintain an inflow design flood control system according to the requirements of this Section.

This plan may be amended at any time provided the revised plan is placed in the facility's operating record as required by Section 257.105(g)(4). This plan must be amended whenever there is a substantial change in conditions or a minimum of every five (5) years.

The Asbury Power Plant maintains one CCR impoundment, the Asbury CCR Impoundment. See Figures 1 and 2 in Appendix I for the Asbury CCR Impoundment location on a topographic map and aerial photograph, respectively.

The Asbury CCR Impoundment is subdivided into three (3) Ponds, identified as the Lower Pond, Upper Pond, and South Pond. The Lower Pond, Upper Pond, and South Pond are separated by interior earthen embankments. The Upper Pond is further subdivided by an interior dike into Upper Pond A (North Cell of the Upper Pond) and Upper Pond B (South Cell of the Upper Pond). The Lower Pond is further subdivided by interior dikes into several sections. The sections of the Lower Pond are identified as Sections D through J for the purposes of this Report. See Figure 3 in Appendix I for a diagram showing each section located within the Asbury CCR Impoundment.

The following sections of this report assess the hydrologic and hydraulic capacity requirements for the Asbury CCR Impoundment.

## **2.0 ANALYSIS OF EXISTING INFLOW DESIGN FLOOD CONTROL SYSTEM**

### **2.1 Hazard Classification and Design Assumptions**

The Asbury CCR Impoundment is classified as a significant hazard potential CCR surface impoundment in accordance with Section 257.73(a)(2) of the CCR Rule. In accordance with Section 257.82(a), the inflow design flood control system must adequately manage flow for a 1,000-year flood.

Design assumptions for the hydrologic and hydraulic model include the following:

1. There is virtually no loss of water through the bottom of the impoundment. Additionally, all sections of the Impoundment and drainage areas outside of the impoundment are modeled as impervious (CN = 98), with the exception of Lower Pond Section J, which has a significant amount of area that is not subject to submersion. The area within Lower Pond Section J that is not subject to submersion was assigned a CN number of 78 for meadow in good condition with hydrologic soil group D. These assumptions are considered conservative.
2. The Asbury Power Plant was officially taken out of service on March 1, 2020. Water levels assumed for the purposes of this analysis are consistent with historic operating levels of the Asbury CCR Impoundment, and are conservative based upon recent field observations and survey data. The water levels used in the model for the Upper Pond A, Upper Pond B, and Lower Pond Section J are 952.5 feet, 953.6 feet, and 928.8 feet, respectively.
3. There is no process water that enters the Asbury CCR Impoundment.
4. The National Weather Service Precipitation Frequency Data Server was used to determine the 1000-year recurrence interval precipitation estimate for the site. The 1,000-year event for the durations of 6 hours, 12 hours, and 24 hours were evaluated. The 24-hour, 1,000-year recurrence interval precipitation event was determined to be the critical design event that produced the maximum peak discharge for the system. For the 24-hour duration the precipitation depth is estimated at 13.6 inches. A copy of the output from the National Weather Service Precipitation Frequency Data Server is included in Appendix II.

Figure 3 in Appendix I is a diagram showing each section located within the Asbury CCR Impoundment, the approximate location of the drainage area for each section, and flow routing.

## **2.2 Hydrologic and Hydraulic Model**

The volumes of the individual basins located within the Asbury CCR Impoundment were estimated using a 1-foot topographic map of the impoundment. The topographic map was developed from a comprehensive topographic survey performed in 2012. The topographic survey was updated in 2014, 2016, and 2020. The August 2020 topographic survey update included surveying of areas in the Lower Pond where additional CCR had been placed.

See Figure 3 in Appendix I for a diagram showing each section located within the Asbury CCR Impoundment, the current topographic contours, the approximate location of the drainage area for each section, and flow routing. The following table provides the model input data used for each section.

<b>Section</b>	<b>Drainage Area (Acres)</b>	<b>Receives Water From</b>	<b>Lowest Elevation on Dike</b>	<b>TR55 CN</b>
Upper Pond A	4.94	NA	953.8	98
Upper Pond B	14.87	NA	954.4	93.42
South Pond (Section C)	12.40	NA	954.2	98
Lower Pond Section D	10.50	Upper Pond A	951.7	98
Lower Pond Section E	7.02	Section D	947.3	98
Lower Pond Section F	3.99	NA	952.8	98
Lower Pond Section G	4.39	NA	946.9	98
Lower Pond Section H	9.51	NA	947.5	98
Lower Pond Section I	12.19	NA	946.5	98
Lower Pond Section J	39.30	Upper Pond B	931.5	86.61

The U.S. Army Corps of Engineers HEC-1 and HEC-HMS software was used to model the flow of water through the connected sections within the impoundment and to estimate the ponding water level in isolated sections within the impoundment. The HEC models are designed to simulate the surface runoff response of a watershed to precipitation by representing the watershed as an interconnected system of hydrologic and hydraulic components. Rainfall over the Asbury CCR Impoundment was modeled using the SCS Unit Hydrograph method. The SCS Type II distribution and abstractions from rainfall were estimated using the NRCS Technical Release 55, Urban Hydrology for Small Watersheds. To be conservative, most of the drainage areas in the model were considered virtually impervious (CN = 98). The exception is Lower Pond Section J, which has a significant area that is not subject to submersion.

Five (5) different HEC models were developed based on the hydraulic connections within the Impoundment, which as summarized below.

- 1. Upper Pond A, Lower Pond Section D, and Lower Pond Section E:** The drainage area for Upper Pond A also includes the coal pile drainage area. The initial water level in Upper Pond A is 952.5 feet. Water discharges from Upper Pond A into Lower Pond Section D from three (3) 10-inch pipes. The intake of two of these pipes is set at 952.16 feet and the intake of the third pipe is set at 953.0 feet. Flow through these three pipes was estimated using Manning’s equation. Water in Lower Pond Section D discharges to Lower Pond Section E from two (2) 10-inch pipes passing through the separating dike. Flow through these two pipes was estimated using Manning’s equation until the pipe inlets became submerged with 2.5 feet of water. With water 2.5 feet or higher over the pipe inlets, flow was

estimated using the Hazen Williams equation for flow under pressure. There are no external discharge spillways from Upper Pond A, Lower Section D, or Lower Pond Section E.

2. **South Pond (Section C):** This basin within the Impoundment was modeled independently because it is relatively isolated from the rest of the Impoundment, and primarily receives water through precipitation. There is no external discharge spillway on the perimeter levee embankment of the South Pond (Section C).
3. **Lower Pond Section F:** This basin within the Impoundment was modeled independently because it is relatively isolated from the rest of the Impoundment, and primarily receives water through precipitation. There are no external discharge spillways from Lower Pond Section F.
4. **Lower Pond Section G:** This basin within the Impoundment was modeled independently because it is relatively isolated from the rest of the Impoundment, and primarily receives water through precipitation. There are overflow pipes from Lower Pond Section G to Lower Pond Section J, but the ponding level in Lower Pond Section G does not reach the pipe inverts under the design flood. There is no external discharge spillway from Lower Pond Section G.
5. **Upper Pond B, Lower Pond Section H, Lower Pond Section I, and Lower Pond Section J:** The initial water level in Upper Pond B was modeled as 953.6 feet. Water discharges from Upper Pond B into Lower Pond Section J from one (1) 10-inch pipe. The intake of this pipe is set at approximately 953.0 feet. Flow through this pipe was estimated using Manning's equation.

Lower Pond Sections H and I overflow into Lower Pond Section J through earthen channel spillways.

The initial water level in Lower Pond Section J is 928.8 feet. Water from Section J is discharged at Outfall #002 through a primary spillway consisting of two (2) 12-inch pipes. The intake of these two (2) pipes is set at approximately 928.8 feet. Flow through these pipes was estimated using Manning's equation.

Outfall #002 also has an auxiliary spillway consisting of a trapezoidal shaped concrete channel that is 24 feet wide and 1.2 feet from the bottom of the spillway to the top of the berm. The flowline of the auxiliary spillway is at elevation 930.35 feet. Flow over the auxiliary spillway was estimated using the equation for flow over an Ogee spillway.



## 2.3 Hydrologic and Hydraulic Modeling Results

Table 2.3-1 below summarizes the results of the modeled stormwater flooding event, including the resulting water elevation and freeboard in each basin.

<b>Section</b>	<b>Result of 1000 Year Rainfall</b>	<b>Computed Water Elevation (ft.)</b>	<b>Freeboard (feet)</b>
Upper Pond A	Flows into Section D	953.45	0.35
Upper Pond B	Flows into Section J	954.14	0.26
South Pond (Section C)	Contains Rainfall	952.39	1.81
Lower Pond Section D	Flows into Section E	951.41	0.29
Lower Pond Section E	Contains Rainfall	946.61	0.69
Lower Pond Section F	Contains Rainfall	950.46	2.34
Lower Pond Section G	Contains Rainfall	941.79 <sup>1</sup>	5.11
Lower Pond Section H	Flows into Section J	947.43	0.07
Lower Pond Section I	Flows into Section J	946.47	0.03
Lower Pond Section J	Discharge to Outfall	931.31	0.19

<sup>1</sup>The computed water elevation for Section G includes 0.90 acre feet of water more than what was calculated in the HEC-1 model. This additional 0.90 acre-feet of water is the maximum daily discharge from the historic pumping of bottom ash sluice water. This is no longer occurring, but is conservative and does not impact the conclusions of this study at this time.

Lower Pond Section E, which is the end basin for flows from the coal pile, Upper Pond A, and Lower Pond Section D, contains the design flood with a freeboard of 0.69 feet below the lowest part of the exterior perimeter levee embankment.

South Pond (Section C) and Lower Pond Sections F, and G are relatively isolated from the other portions of the Impoundment and have sufficient storage volume to contain the precipitation within them without overflowing into an adjacent section. Freeboard in each of these basins is greater than one foot.

Lower Pond Sections H and I have significantly changed since the last update. These Sections will currently overflow into Lower Pond Section J during the design storm. Freeboard in Sections H and I have been reduced to 0.07 feet and 0.03 feet, respectively.

Lower Pond Section J, which is the end basin for flows from the Upper Pond B and Lower Pond Sections H and I, contains the design flood with a freeboard of 0.19 feet below the lowest part of the dike and 0.96 feet over the auxiliary spillway. Note that Lower Pond Section J was modeled with the two (2) outlet pipes open during the storm event.

## 2.4 Conclusions

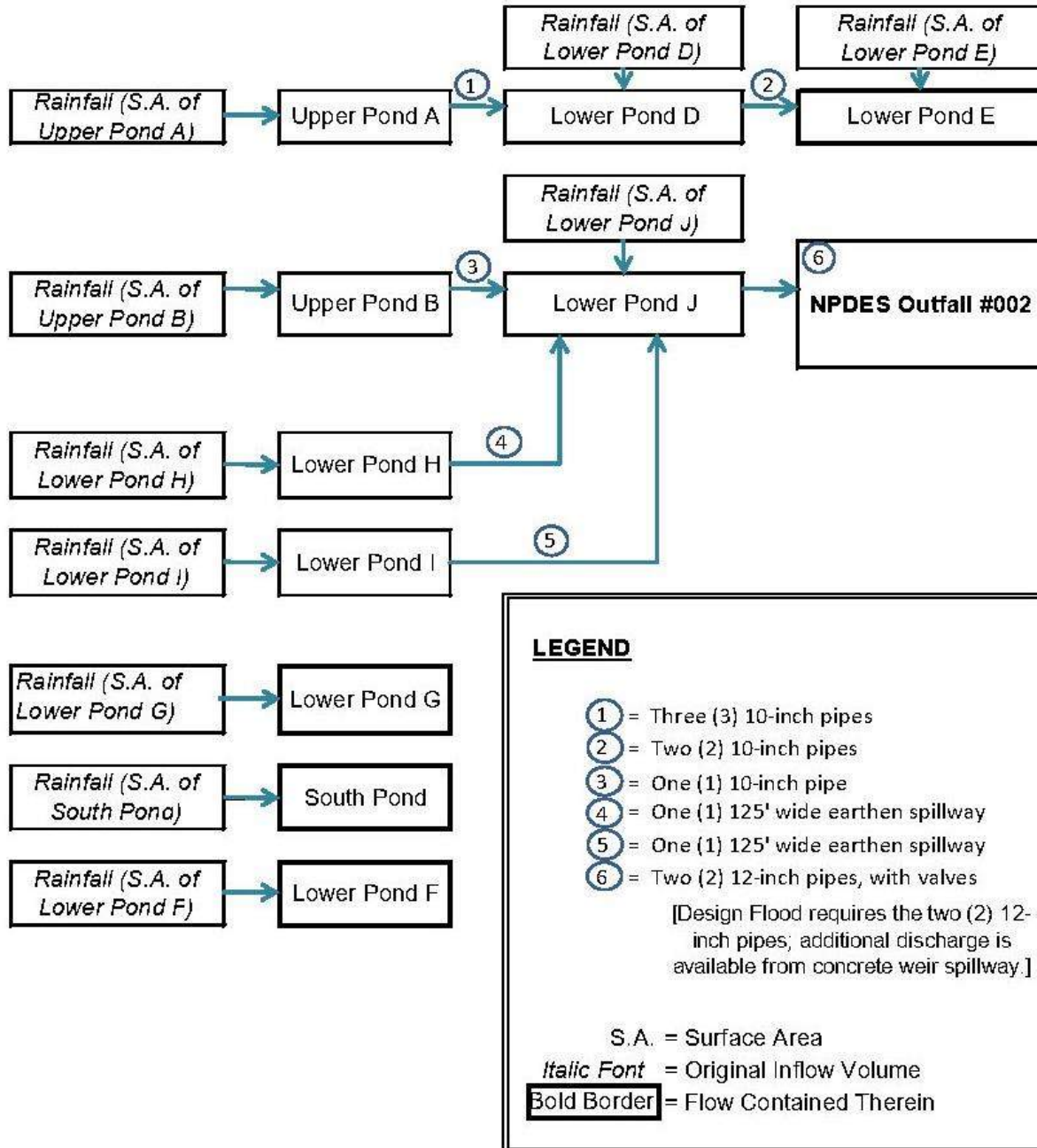
The Asbury CCR Impoundment is capable of adequately managing the Design Flood under existing conditions. The total capacity of the permitted discharge point, NPDES Outfall #002, exceeds what is necessary during the Design Flood event. In addition to the excess capacity of the spillway at NPDES Outfall #002, there is excess storm water storage capacity in several sections of the Impoundment. The Empire District Electric Company has several options available to convey excess storm water by gravity flow or pump excess storm water if necessary.



### 3.0 INFLOW DESIGN FLOOD CONTROL SYSTEM PLAN

The Empire District Electric Company’s Inflow Design Flood Control Plan for the Asbury CCR Impoundment is summarized in the flow chart below. Under typical operating conditions, the Design Flood event is discharged through the two (2) 12-inch outlet pipes in Section J of the Lower Pond, at NPDES Discharge #002.

#### INFLOW DESIGN FLOOD CONTROL SYSTEM PLAN



### 3.1 Contingency Planning

The two (2) 12-inch outlet pipes are regularly observed by The Empire District Electric Company’s staff to verify their functionality. In the event of unanticipated conditions, such as obstruction of one or more of these discharge pipes, or a storm event that exceeds the Design Flood event, The Empire District Electric Company can make several different operational adjustments for routing of additional storm water. Some of these operational adjustments are summarized in the list below.

As previously stated, the Asbury CCR Impoundment passes the Design Flood event under normal operating conditions. The options listed below are presented for contingency planning purposes only and are not explicitly incorporated into the Inflow Design Flood Control System Plan.

1. Additional storm water flow capacity is available from the auxiliary concrete spillway at NPDES Outfall #002, in Lower Pond Section J.
2. Additional storm water storage is available in the South Pond (Section C). Water can be conveyed to the South Pond from Upper Pond B by opening of one or both of the two (2) 12-inch pipes with valves between Upper Pond B and the South Pond.

### 4.0 CCR RULE SECTION 257.82(c)(5) – CERTIFICATION

The undersigned Professional Engineer certifies that the Inflow Design Flood Control System Plan meets the requirements of 40 CFR 257.82.

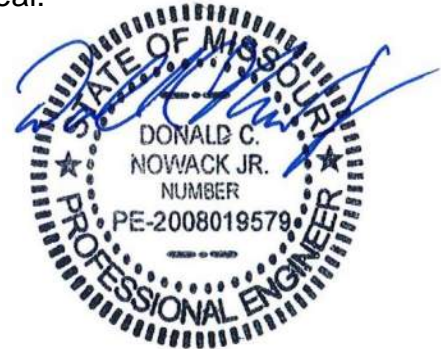
State of Missouri Professional Engineering License Number: 2008019579

Name: Donald C. Nowack, P.E.

Seal:

Signature: 

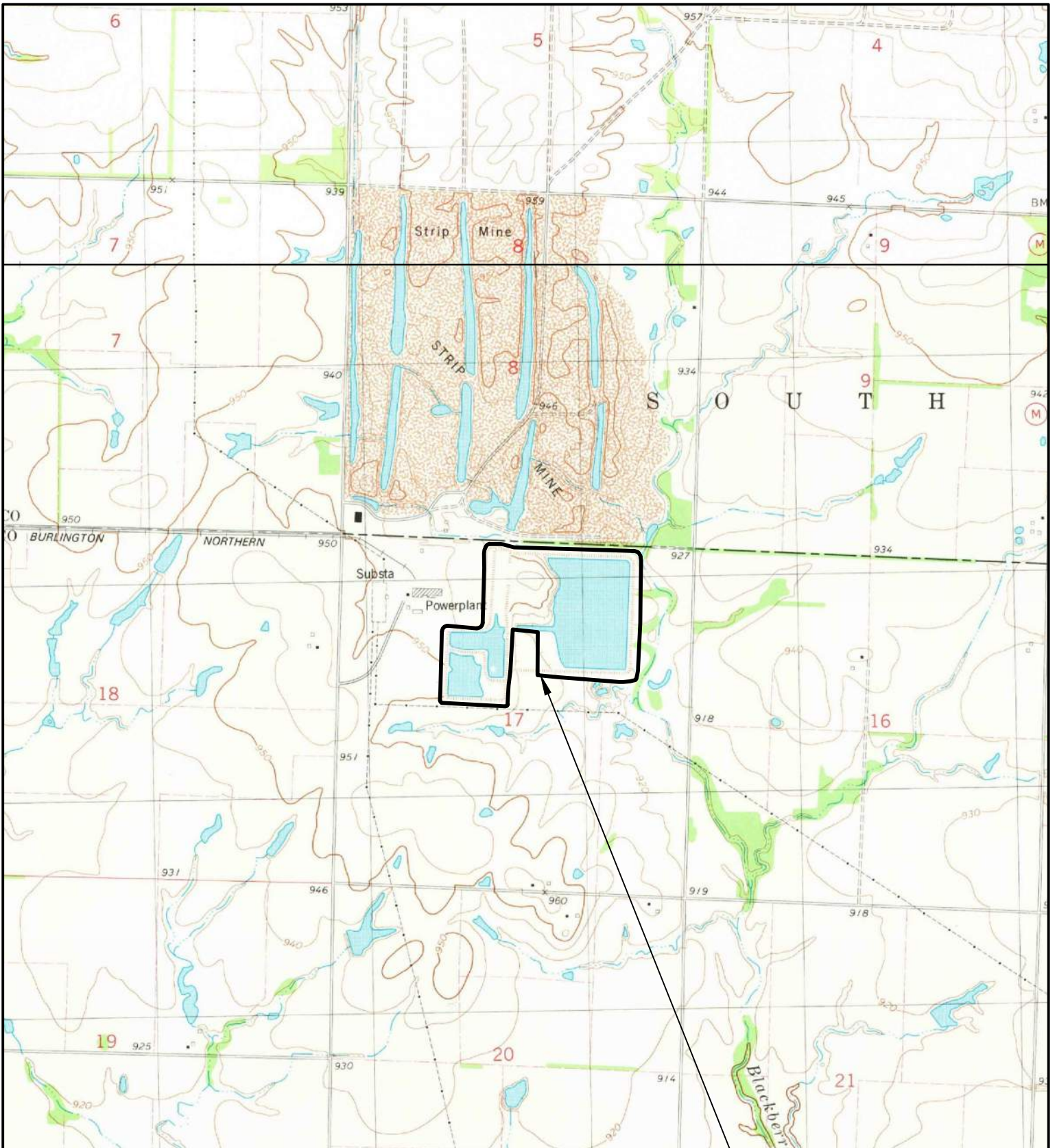
Date: October 15, 2021



10/15/21



**APPENDIX I**  
**FIGURES**



USGS Asbury 7.5 Minute Topographic Quadrangle, 1981  
 USGS Mindenmines 7.5 Minute Topographic Quadrangle, 1981

Asbury CCR Impoundment

Project: Asbury Power Plant, 21133 Uphill Lane, Asbury, MO  
 Client: Empire District Electric Company

### Site Location on Topographic Map

DATE: October 15, 2021

Project Number: 231518

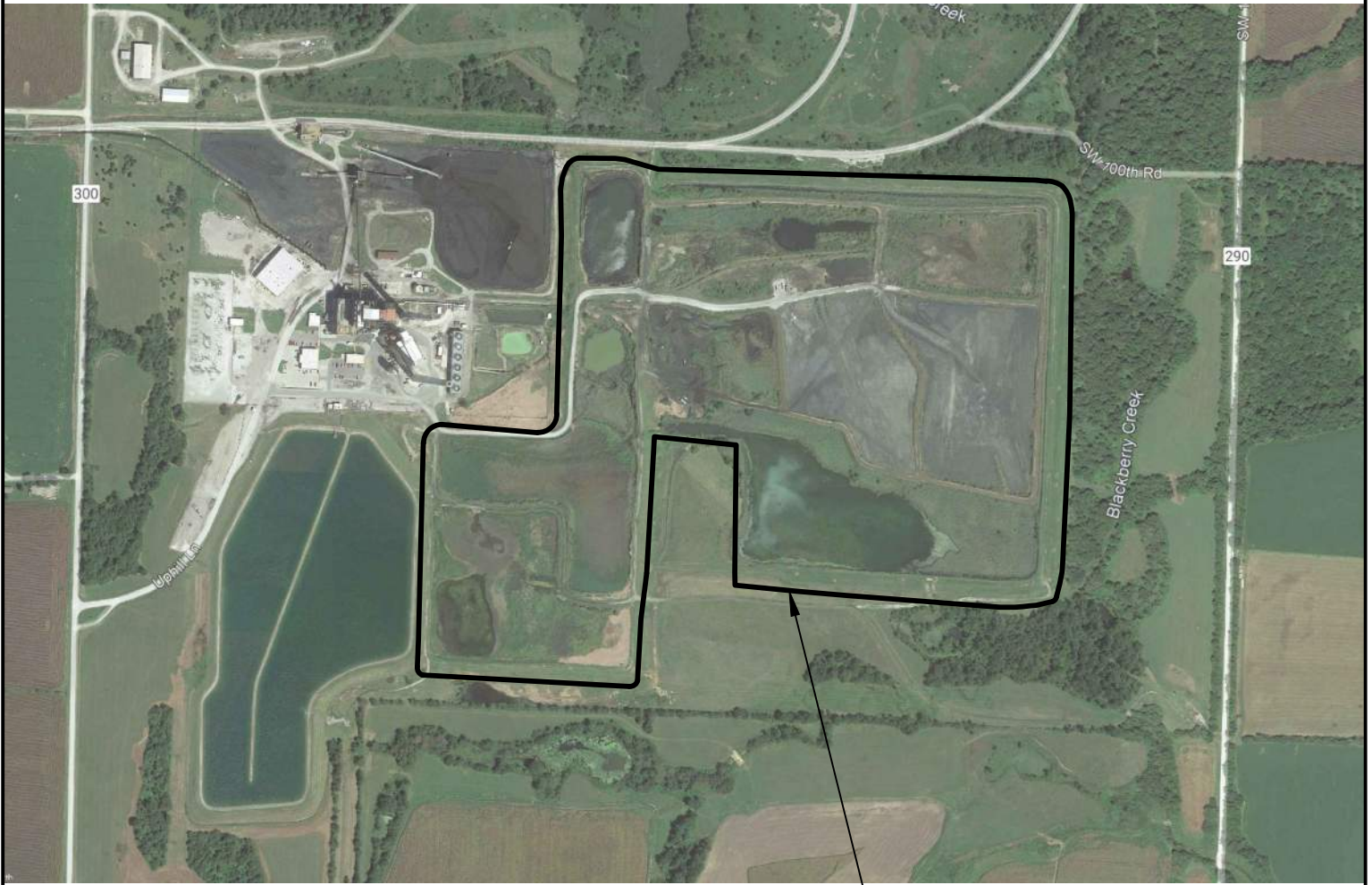


SCALE  
 1" = 2000'

**PPI** PALMERTON & PARRISH, INC.  
 GEOTECHNICAL AND MATERIALS ENGINEERS/MATERIALS TESTING LABORATORIES/ENVIRONMENTAL SERVICES

FIGURE 1





Asbury CCR Impoundment



SCALE  
1"=800'

Project: Asbury Power Plant, 21133 Uphill Lane, Asbury, MO  
Client: Empire District Electric Company

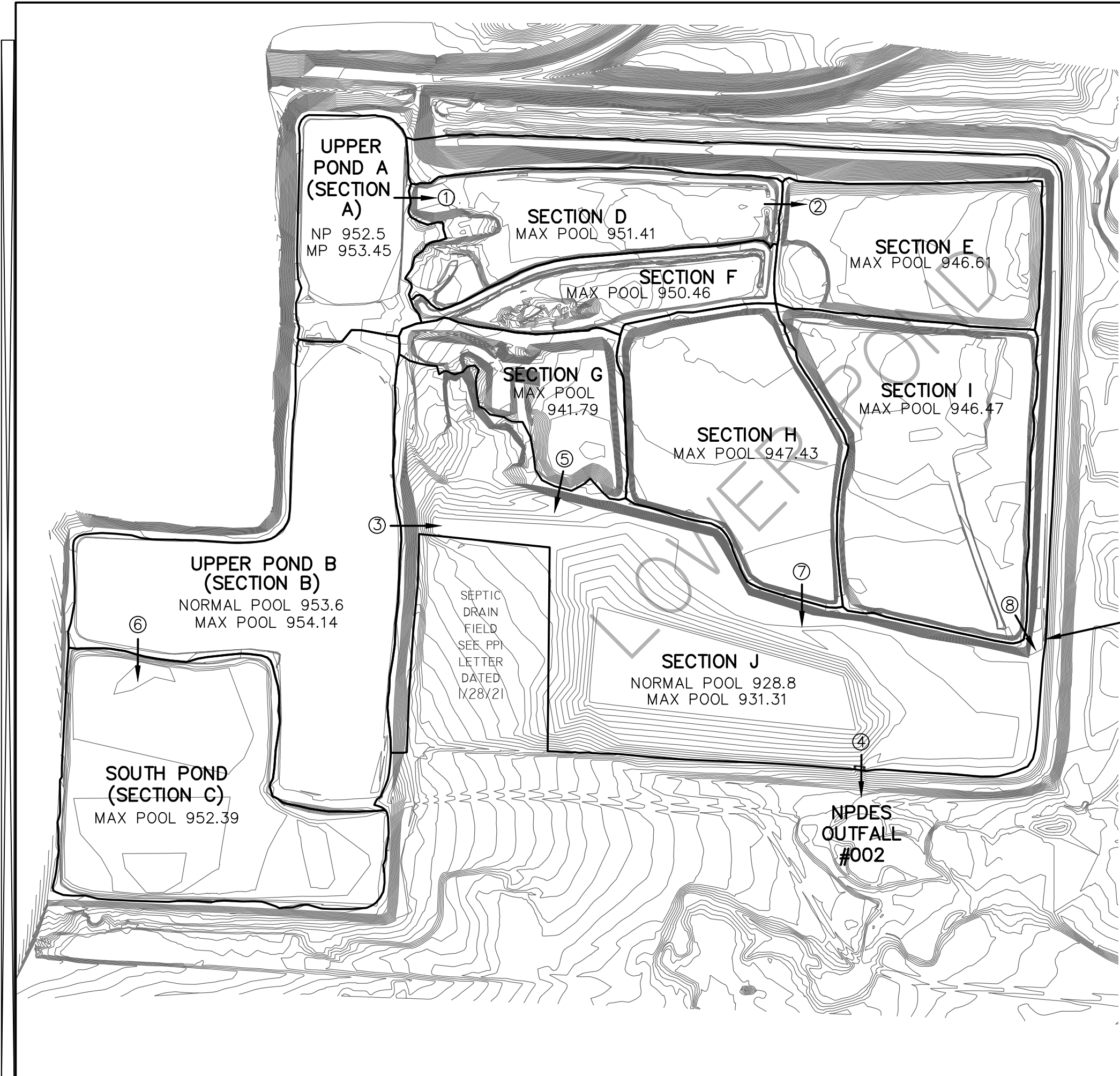
### Site Location on 2017 Aerial Photograph

DATE: October 15, 2021

Project Number: 231518

**PPI** PALMERTON & PARRISH, INC.  
GEOTECHNICAL AND MATERIALS ENGINEERS/MATERIALS TESTING LABORATORIES/ENVIRONMENTAL SERVICES

FIGURE 2



**UPPER POND A  
(SECTION A)**  
NP 952.5  
MP 953.45

**SECTION D**  
MAX POOL 951.41

**SECTION E**  
MAX POOL 946.61

**SECTION F**  
MAX POOL 950.46

**SECTION G**  
MAX POOL 941.79

**SECTION I**  
MAX POOL 946.47

**SECTION H**  
MAX POOL 947.43

**UPPER POND B  
(SECTION B)**  
NORMAL POOL 953.6  
MAX POOL 954.14

SEPTIC DRAIN FIELD  
SEE PPI LETTER DATED 1/28/21

**SECTION J**  
NORMAL POOL 928.8  
MAX POOL 931.31

**SOUTH POND  
(SECTION C)**  
MAX POOL 952.39

NPDES  
OUTFALL  
#002

SCALE  
1" = 300'

Project: Asbury Power Plant, 21133 Uphill Lane, Asbury, Missouri  
Client: Empire District Electric Company

**Asbury CCR Impoundment**

DATE: October 15, 2021

Project Number: 231518

**PPI PALMERTON & PARRISH, INC.**  
GEOTECHNICAL AND MATERIALS ENGINEERS / MATERIALS TESTING LABORATORIES / ENVIRONMENTAL SERVICES

**FIGURE 3**

- ① 3-10" PIPES THROUGH DIKE
- ② 2-10" PIPES THROUGH DIKE
- ③ 1-10" PIPE THROUGH DIKE
- ④ NPDES OUTFALL #002  
PRIMARY SPILLWAY: 2-12" PIPES WITH VALVES THROUGH DIKE  
AUXILIARY SPILLWAY: 24' WIDE CONCRETE SPILLWAY ON TOP OF DIKE
- ⑤ 3-12" PIPES THROUGH DIKE
- ⑥ 2-12" PIPES WITH VALVES THROUGH DIKE
- ⑦ 125' WIDE EARTHEN SPILLWAY ON TOP OF DIKE
- ⑧ 125' WIDE EARTHEN SPILLWAY ON TOP OF DIKE

SECTION DRAINAGE AREA BOUNDARY



**APPENDIX II**  
**PRECIPITATION TABLE & PIPE FLOW CALCULATIONS**





**NOAA Atlas 14, Volume 8, Version 2**  
**Location name: Asbury, Missouri, USA\***  
**Latitude: 37.3608°, Longitude: -94.5889°**  
**Elevation: 941.17 ft\*\***  
 \* source: ESRI Maps  
 \*\* source: USGS



**POINT PRECIPITATION FREQUENCY ESTIMATES**

Sanja Perica, Deborah Martin, Sandra Pavlovic, Ishani Roy, Michael St. Laurent, Carl Trypaluk,  
 Dale Unruh, Michael Yekta, Geoffery Bonnin

NOAA, National Weather Service, Silver Spring, Maryland

[PF\\_tabular](#) | [PF\\_graphical](#) | [Maps & aeriels](#)

**PF tabular**

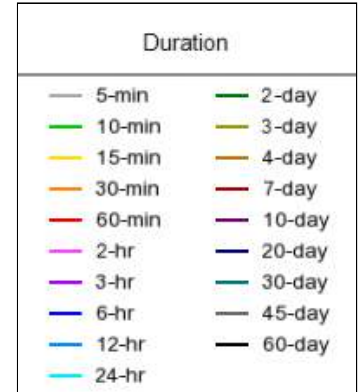
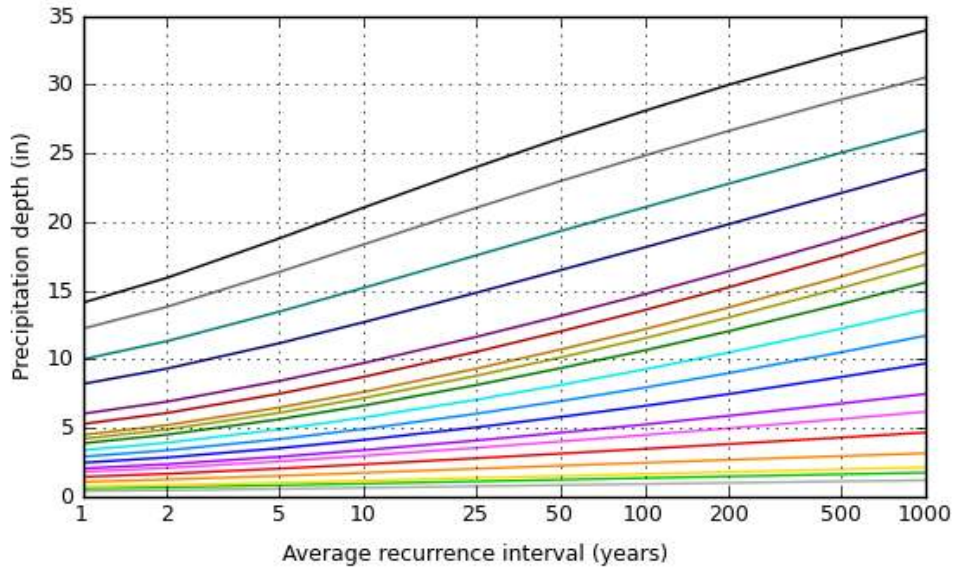
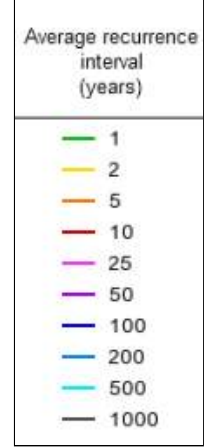
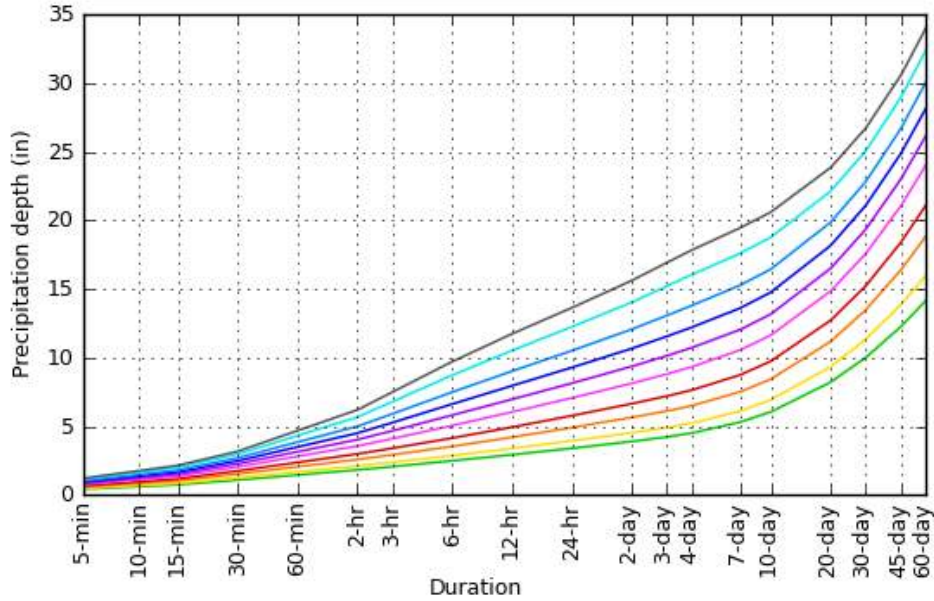
<b>PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches)<sup>1</sup></b>										
<b>Duration</b>	<b>Average recurrence interval (years)</b>									
	<b>1</b>	<b>2</b>	<b>5</b>	<b>10</b>	<b>25</b>	<b>50</b>	<b>100</b>	<b>200</b>	<b>500</b>	<b>1000</b>
<b>5-min</b>	<b>0.415</b> (0.326-0.517)	<b>0.476</b> (0.374-0.594)	<b>0.575</b> (0.451-0.720)	<b>0.657</b> (0.513-0.824)	<b>0.767</b> (0.582-0.981)	<b>0.850</b> (0.634-1.10)	<b>0.932</b> (0.678-1.23)	<b>1.01</b> (0.715-1.36)	<b>1.12</b> (0.767-1.54)	<b>1.20</b> (0.806-1.67)
<b>10-min</b>	<b>0.607</b> (0.478-0.758)	<b>0.697</b> (0.548-0.870)	<b>0.843</b> (0.661-1.05)	<b>0.961</b> (0.751-1.21)	<b>1.12</b> (0.852-1.44)	<b>1.25</b> (0.929-1.61)	<b>1.36</b> (0.993-1.80)	<b>1.49</b> (1.05-2.00)	<b>1.64</b> (1.12-2.25)	<b>1.76</b> (1.18-2.45)
<b>15-min</b>	<b>0.741</b> (0.583-0.924)	<b>0.850</b> (0.669-1.06)	<b>1.03</b> (0.806-1.28)	<b>1.17</b> (0.916-1.47)	<b>1.37</b> (1.04-1.75)	<b>1.52</b> (1.13-1.96)	<b>1.67</b> (1.21-2.19)	<b>1.81</b> (1.28-2.44)	<b>2.00</b> (1.37-2.75)	<b>2.15</b> (1.44-2.99)
<b>30-min</b>	<b>1.08</b> (0.854-1.35)	<b>1.25</b> (0.987-1.57)	<b>1.53</b> (1.20-1.91)	<b>1.75</b> (1.36-2.19)	<b>2.04</b> (1.55-2.61)	<b>2.26</b> (1.69-2.92)	<b>2.48</b> (1.80-3.26)	<b>2.69</b> (1.90-3.62)	<b>2.97</b> (2.02-4.07)	<b>3.17</b> (2.12-4.41)
<b>60-min</b>	<b>1.45</b> (1.14-1.81)	<b>1.68</b> (1.32-2.10)	<b>2.05</b> (1.61-2.57)	<b>2.37</b> (1.85-2.97)	<b>2.80</b> (2.13-3.60)	<b>3.14</b> (2.35-4.08)	<b>3.49</b> (2.54-4.61)	<b>3.84</b> (2.71-5.18)	<b>4.32</b> (2.95-5.94)	<b>4.68</b> (3.14-6.52)
<b>2-hr</b>	<b>1.82</b> (1.45-2.25)	<b>2.10</b> (1.67-2.60)	<b>2.58</b> (2.04-3.19)	<b>2.98</b> (2.35-3.71)	<b>3.56</b> (2.75-4.55)	<b>4.02</b> (3.04-5.19)	<b>4.50</b> (3.31-5.91)	<b>4.99</b> (3.56-6.70)	<b>5.67</b> (3.91-7.76)	<b>6.19</b> (4.18-8.57)
<b>3-hr</b>	<b>2.06</b> (1.65-2.53)	<b>2.37</b> (1.90-2.92)	<b>2.92</b> (2.33-3.59)	<b>3.40</b> (2.69-4.20)	<b>4.09</b> (3.18-5.23)	<b>4.67</b> (3.55-6.01)	<b>5.26</b> (3.90-6.91)	<b>5.90</b> (4.23-7.91)	<b>6.79</b> (4.71-9.28)	<b>7.49</b> (5.08-10.3)
<b>6-hr</b>	<b>2.48</b> (2.01-3.02)	<b>2.86</b> (2.31-3.48)	<b>3.53</b> (2.85-4.31)	<b>4.14</b> (3.32-5.07)	<b>5.05</b> (3.98-6.42)	<b>5.81</b> (4.47-7.44)	<b>6.62</b> (4.96-8.64)	<b>7.49</b> (5.42-9.98)	<b>8.72</b> (6.11-11.9)	<b>9.71</b> (6.63-13.3)
<b>12-hr</b>	<b>2.92</b> (2.39-3.52)	<b>3.38</b> (2.76-4.08)	<b>4.20</b> (3.42-5.07)	<b>4.93</b> (4.00-5.98)	<b>6.04</b> (4.81-7.61)	<b>6.96</b> (5.42-8.85)	<b>7.95</b> (6.01-10.3)	<b>9.01</b> (6.58-11.9)	<b>10.5</b> (7.43-14.2)	<b>11.7</b> (8.07-16.0)
<b>24-hr</b>	<b>3.39</b> (2.80-4.04)	<b>3.94</b> (3.25-4.70)	<b>4.90</b> (4.04-5.86)	<b>5.77</b> (4.73-6.92)	<b>7.06</b> (5.67-8.81)	<b>8.13</b> (6.39-10.2)	<b>9.28</b> (7.07-11.9)	<b>10.5</b> (7.73-13.8)	<b>12.2</b> (8.70-16.4)	<b>13.6</b> (9.44-18.4)
<b>2-day</b>	<b>3.89</b> (3.25-4.59)	<b>4.53</b> (3.78-5.35)	<b>5.64</b> (4.70-6.68)	<b>6.64</b> (5.50-7.89)	<b>8.13</b> (6.59-10.0)	<b>9.36</b> (7.42-11.7)	<b>10.7</b> (8.20-13.6)	<b>12.1</b> (8.94-15.7)	<b>14.0</b> (10.0-18.7)	<b>15.6</b> (10.9-21.0)
<b>3-day</b>	<b>4.22</b> (3.55-4.95)	<b>4.90</b> (4.12-5.76)	<b>6.11</b> (5.12-7.19)	<b>7.19</b> (5.99-8.49)	<b>8.80</b> (7.18-10.8)	<b>10.1</b> (8.07-12.6)	<b>11.5</b> (8.93-14.6)	<b>13.1</b> (9.73-16.9)	<b>15.2</b> (10.9-20.2)	<b>16.9</b> (11.8-22.6)
<b>4-day</b>	<b>4.50</b> (3.80-5.26)	<b>5.22</b> (4.41-6.11)	<b>6.49</b> (5.46-7.61)	<b>7.63</b> (6.39-8.98)	<b>9.32</b> (7.63-11.4)	<b>10.7</b> (8.57-13.2)	<b>12.2</b> (9.47-15.4)	<b>13.8</b> (10.3-17.8)	<b>16.0</b> (11.6-21.2)	<b>17.8</b> (12.5-23.8)
<b>7-day</b>	<b>5.30</b> (4.52-6.14)	<b>6.10</b> (5.20-7.08)	<b>7.50</b> (6.37-8.72)	<b>8.73</b> (7.38-10.2)	<b>10.5</b> (8.70-12.8)	<b>12.0</b> (9.70-14.7)	<b>13.6</b> (10.6-17.0)	<b>15.3</b> (11.5-19.6)	<b>17.6</b> (12.8-23.1)	<b>19.4</b> (13.7-25.8)
<b>10-day</b>	<b>6.04</b> (5.18-6.97)	<b>6.92</b> (5.93-7.99)	<b>8.43</b> (7.20-9.74)	<b>9.74</b> (8.27-11.3)	<b>11.6</b> (9.63-14.0)	<b>13.2</b> (10.6-16.0)	<b>14.8</b> (11.6-18.4)	<b>16.4</b> (12.4-21.0)	<b>18.8</b> (13.7-24.5)	<b>20.6</b> (14.6-27.2)
<b>20-day</b>	<b>8.21</b> (7.13-9.37)	<b>9.34</b> (8.09-10.7)	<b>11.2</b> (9.65-12.8)	<b>12.7</b> (10.9-14.6)	<b>14.8</b> (12.4-17.5)	<b>16.5</b> (13.4-19.8)	<b>18.2</b> (14.3-22.3)	<b>19.9</b> (15.1-25.0)	<b>22.1</b> (16.2-28.6)	<b>23.8</b> (17.0-31.3)
<b>30-day</b>	<b>10.0</b> (8.74-11.3)	<b>11.3</b> (9.89-12.9)	<b>13.5</b> (11.7-15.3)	<b>15.2</b> (13.2-17.4)	<b>17.6</b> (14.7-20.6)	<b>19.3</b> (15.8-23.0)	<b>21.1</b> (16.7-25.6)	<b>22.8</b> (17.4-28.5)	<b>25.0</b> (18.4-32.2)	<b>26.7</b> (19.1-34.9)
<b>45-day</b>	<b>12.2</b> (10.8-13.8)	<b>13.8</b> (12.2-15.6)	<b>16.4</b> (14.3-18.5)	<b>18.4</b> (16.0-20.9)	<b>21.0</b> (17.6-24.4)	<b>23.0</b> (18.9-27.1)	<b>24.8</b> (19.8-30.0)	<b>26.7</b> (20.4-33.1)	<b>28.9</b> (21.3-36.9)	<b>30.5</b> (22.0-39.8)
<b>60-day</b>	<b>14.1</b> (12.5-15.8)	<b>15.9</b> (14.1-17.9)	<b>18.8</b> (16.5-21.2)	<b>21.1</b> (18.4-23.8)	<b>24.0</b> (20.2-27.7)	<b>26.1</b> (21.5-30.6)	<b>28.1</b> (22.4-33.8)	<b>30.0</b> (23.0-37.1)	<b>32.3</b> (23.9-41.1)	<b>34.0</b> (24.5-44.1)

<sup>1</sup> Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS). Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values. Please refer to NOAA Atlas 14 document for more information.

[Back to Top](#)

### PF graphical

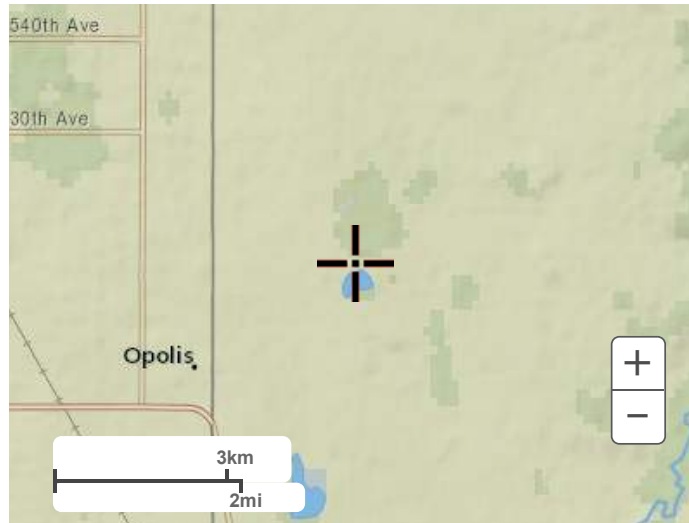
PDS-based depth-duration-frequency (DDF) curves  
 Latitude: 37.3608°, Longitude: -94.5889°



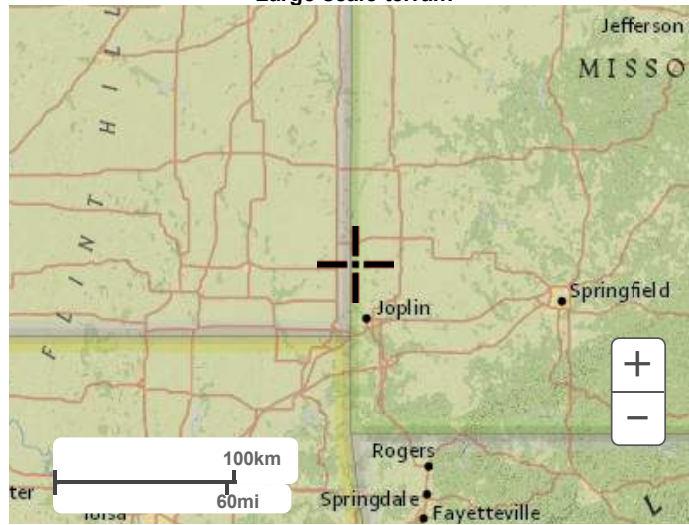
[Back to Top](#)

### Maps & aerials

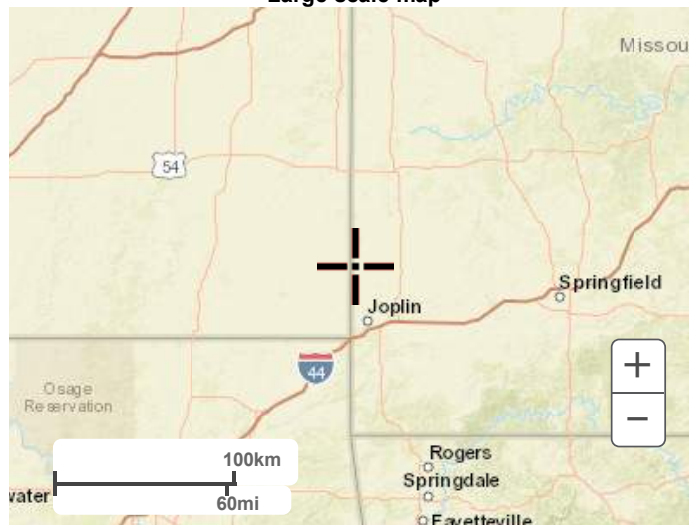
Small scale terrain



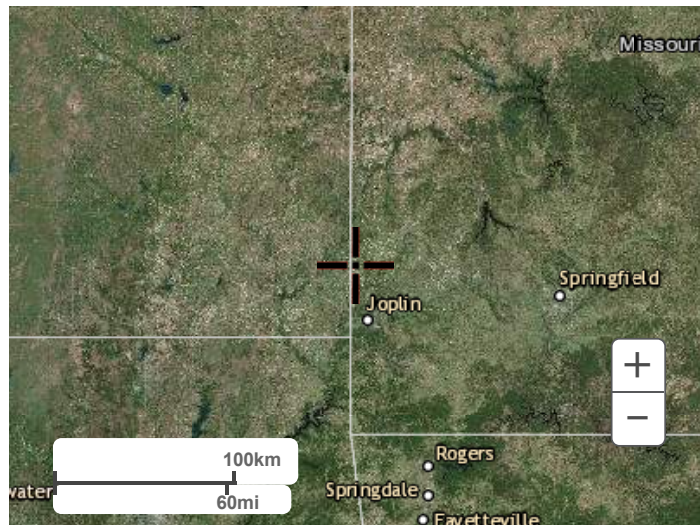
Large scale terrain



Large scale map



Large scale aerial



[Back to Top](#)

---

[US Department of Commerce](#)  
[National Oceanic and Atmospheric Administration](#)  
[National Weather Service](#)  
[National Water Center](#)  
1325 East West Highway  
Silver Spring, MD 20910  
Questions?: [HDSC.Questions@noaa.gov](mailto:HDSC.Questions@noaa.gov)

[Disclaimer](#)

Asbury CCR Impoundment - Pipe Flow Calculations

Manning's Equation  $V = (Cf/n) R^{0.67} S^{0.5}$

$Q = VA$

V = Velocity (ft/sec) Cf = Conversion factor S = Slope

Q = Flow (cu ft/sec) n = Pipe roughness coefficient

R = Hydraulic Radius (ft) = Area (A) / Wetted Perimeter (P)

Upper Pond A to Section D

Q	5.82	cfs
V	10.68	fps
Pipe Dia	10	in
	0.83	ft
n	0.012	PVC
Cf	1.49	
A	0.55	sq ft
P	2.62	ft
S	0.06	
R	0.21	ft

Section D to Section E

Q	4.76	cfs
V	8.72	fps
Pipe Dia	10	in
	0.83	ft
n	0.012	PVC
Cf	1.49	
A	0.55	sq ft
P	2.62	ft
S	0.04	
R	0.21	ft

Section G to Lower Pond J

Q	11.21	cfs
V	14.27	fps
Pipe Dia	12	in
	1	ft
n	0.012	PVC
Cf	1.49	
A	0.79	sq ft
P	3.14	ft
S	0.084	
R	0.25	ft

Upper Pond B to Lower Pond J

Q	3.36	cfs
V	6.17	fps
Pipe Dia	10	in
	0.83	ft
n	0.012	PVC
Cf	1.49	
A	0.55	sq ft
P	2.62	ft
S	0.02	
R	0.21	ft

Outlet - Outfall 002

Q	5.47	cfs
V	6.97	fps
Pipe Dia	12	in
	1	ft
n	0.012	PVC
Cf	1.49	
A	0.79	sq ft
P	3.14	ft
S	0.02	
R	0.25	ft

## Asbury CCR Impoundment - Pipe Flow Calculations

Hazen Williams Equation for Flow

$$Q = 0.285 C (D^{2.63})(S^{0.54})$$

Q = Flow (cu ft/sec)

C = Hazen Williams Friction Coefficient (140 for PVC)

D = Pipe Diameter (ft)

S = Hydraulic Grade Line Slope = Water Height/Pipe Length (50')

Pressure flow from 10" pipe between Section D and Section E.

Water Height	S	Q	Water Elev
2.5	0.05	4.895	951
3.5	0.07	5.870	952



**APPENDIX III**  
**HEC OUTPUT**





**APPENDIX III-1**  
**HEC-1 OUTPUT**  
**UPPER POND A, SECTION D, & SECTION E**

\*\*\*\*\*
FLOOD HYDROGRAPH PACKAGE (HEC-1)
JUN 1998
VERSION 4.1
RUN DATE 12OCT16 TIME 10:12:46
\*\*\*\*\*

\*\*\*\*\*
U. S. ARMY CORPS OF ENGINEERS
HYDROLOGIC ENGINEERING CENTER
609 SECOND STREET
DAVIS, CALIFORNIA 95616
(916) 756-1104
\*\*\*\*\*

X X XXXXXX XXXX X
X X X X X XX
X X X X X X
XXXXXXXX XXXX X XXXX X
X X X X X X
X X XXXXXX XXXX XXX

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.
THE DEFINITION OF -MISK- ON R/CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION
NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,
DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL, LOSS RATE: GREEN AND AMPT INFILTRATION
KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1 HEC-1 INPUT PAGE 1
LINE ID 1 2 3 4 5 6 7 8 9 10
1 ID \*\*\*\*\*
2 ID PROJECT NAME: EDE ASBURY
3 ID CONSULTANT: PALMERTON & PARRISH, INC.
4 ID PROJECT NUMBER: 231518
5 ID DESIGN ENGINEER: DONALD C. NOWACK, P. E.
6 ID FILE NAME: ADE.TXT
7 ID DATE: OCTOBER 17, 2016

Appendix III-1
Page 1 of 24

37 PC 0.9018 0.9038 0.9058 0.9078 0.9097 0.9117 0.9136 0.9155 0.9173 0.9192
38 PC 0.9210 0.9228 0.9245 0.9263 0.9280 0.9297 0.9313 0.9330 0.9346 0.9362
39 PC 0.9377 0.9393 0.9408 0.9423 0.9438 0.9452 0.9466 0.9480 0.9493 0.9507
HEC-1 INPUT PAGE 2

LINE ID 1 2 3 4 5 6 7 8 9 10
40 PC 0.9520 0.9533 0.9546 0.9559 0.9572 0.9584 0.9597 0.9610 0.9622 0.9635
41 PC 0.9647 0.9660 0.9672 0.9685 0.9697 0.9709 0.9722 0.9734 0.9746 0.9758
42 PC 0.9770 0.9782 0.9794 0.9806 0.9818 0.9829 0.9841 0.9853 0.9864 0.9876
43 PC 0.9887 0.9899 0.9910 0.9922 0.9933 0.9944 0.9956 0.9967 0.9978 0.9989
44 PC 1.0000
\* SCS CURVE NUMBER: 98.00
45 LS 98.00
\* TIME OF CONCENTRATION: 0.0833 HR (LAG TIME = 0.6 \* Tc = 0.0500 HR)
46 UD 0.0500
47 KK UPA
48 KM UPPER POND A
49 RS 1 ELEV 0953.0
50 SA 3.4086 3.5908
51 SE 953.0 954.0
52 SD 11.640 17.460
53 SE 953.0 954.0
\* 1 2 3 4 5 6 7 8 9 10
54 KK SECD
55 KM SECTION D
56 PB 1.00
\* DRAINAGE AREA: 6.52 ACRES = 0.0102 SQ. MI.
57 BA 0.0102
\* SCS CURVE NUMBER: 98.00
58 LS 98.00
\* TIME OF CONCENTRATION: 0.0833 HR (LAG TIME = 0.6 \* Tc = 0.0500 HR)
59 UD 0.0500
\* 1 2 3 4 5 6 7 8 9 10
60 KK COMB
61 KM COMBINATION OF SUB BASINS KK
62 HC 2 KM
\* 1 2 3 4 5 6 7 8 9 10
63 KK BASND
64 KM BASIN IN SECTION D
65 RS 1 ELEV 0947.0

Appendix III-1
Page 3 of 24

8 ID RETURN FREQUENCY: 1000-YEAR, 24 HR
9 ID ABSTRACTION TECHNIQUE: SCS CURVE NUMBER
10 ID SCENARIO: UPPER POND A FLOWING INTO SECTIONS D AND E
11 ID \*\*\*\*\*
\* 1 2 3 4 5 6 7 8 9 10
\* NUMBER OF 1 MIN INTERVALS USED FOR CALCULATION
\* \*\*\*NO OF INTERVALS\*1-060 2-120 3-180 6-360 12-720 18-1080 24-1440
IT 1 1440
\* NUMBER OF MIN IN EACH TIME INTERVAL
\* \*\*\*MIN IN INTERVAL\*\*\*1hr-3 2hr-6 3hr-9 6hr-18 12hr-36 18-54 24-72
IN 72
IO 4 0
\*DIAGRAM \*\*\*\*\*
\* 1 2 3 4 5 6 7 8 9 10
JR PREC 13.60
\* STORM DISTRIBUTION: SCS TYPE II
\* STORM DURATION: 24 HOUR
\* 1 2 3 4 5 6 7 8 9 10
16 KK UPA
17 KM COAL PILE AND UPPER POND A
18 PB 1.00
\* DRAINAGE AREA: 24.08 ACRES = 0.0376 SQ. MI.
19 BA 0.0376
\* RAINFALL DISTRIBUTION
20 PC 0.0000 0.0010 0.0020 0.0030 0.0041 0.0051 0.0062 0.0072 0.0083 0.0094
21 PC 0.0105 0.0116 0.0127 0.0138 0.0150 0.0161 0.0173 0.0184 0.0196 0.0208
22 PC 0.0220 0.0232 0.0244 0.0257 0.0269 0.0281 0.0294 0.0306 0.0319 0.0332
23 PC 0.0345 0.0358 0.0371 0.0384 0.0398 0.0411 0.0425 0.0439 0.0452 0.0466
24 PC 0.0480 0.0494 0.0508 0.0523 0.0538 0.0553 0.0568 0.0583 0.0598 0.0614
25 PC 0.0630 0.0646 0.0662 0.0679 0.0696 0.0712 0.0730 0.0747 0.0764 0.0782
26 PC 0.0800 0.0818 0.0836 0.0855 0.0874 0.0892 0.0912 0.0931 0.0950 0.0970
27 PC 0.0990 0.1010 0.1030 0.1051 0.1072 0.1093 0.1114 0.1135 0.1156 0.1178
28 PC 0.1200 0.1222 0.1246 0.1270 0.1296 0.1322 0.1350 0.1379 0.1408 0.1438
29 PC 0.1470 0.1502 0.1534 0.1566 0.1598 0.1630 0.1663 0.1697 0.1733 0.1771
30 PC 0.1810 0.1851 0.1895 0.1941 0.1989 0.2040 0.2094 0.2152 0.2214 0.2280
31 PC 0.2350 0.2427 0.2513 0.2609 0.2715 0.2830 0.3068 0.3544 0.4308 0.5679
32 PC 0.6630 0.6820 0.6986 0.7130 0.7252 0.7350 0.7434 0.7514 0.7588 0.7656
33 PC 0.7720 0.7780 0.7835 0.7890 0.7942 0.7990 0.8036 0.8080 0.8122 0.8162
34 PC 0.8200 0.8237 0.8273 0.8308 0.8342 0.8375 0.8409 0.8442 0.8474 0.8505
35 PC 0.8535 0.8565 0.8594 0.8622 0.8649 0.8676 0.8702 0.8728 0.8753 0.8777
36 PC 0.8800 0.8823 0.8845 0.8868 0.8890 0.8912 0.8934 0.8955 0.8976 0.8997

Appendix III-1
Page 2 of 24

66 SA 0.7216 1.9397 4.2220 4.7966 5.0074 5.1685
67 SE 947.0 948.0 949.0 950.0 951.0 952.0
68 SD 0.0000 0.0000 9.52 9.79 11.74
69 SE 947.0 948.0 949.0 950.0 951.0 952.0
\* 1 2 3 4 5 6 7 8 9 10
70 KK SECE
71 KM SECTION E
72 PB 1.00
\* DRAINAGE AREA: 7.02 ACRES = 0.0110 SQ. MI.
73 BA 0.0110
\* SCS CURVE NUMBER: 98.00
74 LS 98.00
\* TIME OF CONCENTRATION: 0.0833 HR (LAG TIME = 0.6 \* Tc = 0.0500 HR)
75 UD 0.0500
1 HEC-1 INPUT PAGE 3
LINE ID 1 2 3 4 5 6 7 8 9 10
76 KK COMB
77 KM COMBINATION OF SUB BASINS KK
78 HC 2 KM
\* 1 2 3 4 5 6 7 8 9 10
79 KK BASNE
80 KM BASIN IN SECTION E
81 RS 1 ELEV 0939.0
82 SA 0.0936 0.3554 0.8310 2.1810 4.4409 5.2631 5.4799 5.6485 5.8193 5.9915
83 SE 939.0 940.0 941.0 942.0 943.0 944.0 945.0 946.0 947.0 948.0
84 SD 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000
85 SE 939.0 940.0 941.0 942.0 943.0 944.0 945.0 946.0 947.0 948.0
\* 1 2 3 4 5 6 7 8 9 10
86 ZZ

1 SCHEMATIC DIAGRAM OF STREAM NETWORK
INPUT LINE (V) ROUTING (--->) DIVERSION OR PUMP FLOW
NO. (.) CONNECTOR (-----) RETURN OF DIVERTED OR PUMPED FLOW
16 UPA
V

Appendix III-1
Page 4 of 24

```

47      V
      UPA
      .
54      .       SECD
      .
60      COMB.....
      V
63      BASND
      .
70      .       SECE
      .
76      COMB.....
      V
79      BASNE

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION
*-----*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* JUN 1998 *
* VERSION 4.1 *
* RUN DATE 12OCT16 TIME 10:12:46 *
*-----*

```

```

*-----*
* U. S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
*-----*

```

```

*-----*
PROJECT NAME: EDE ASBURY
CONSULTANT: PALMERTON & PARRISH, INC.
PROJECT NUMBER: 231518
DESIGN ENGINEER: DONALD C. NOWACK, P. E.
FILE NAME: ADE.TXT
DATE: OCTOBER 17, 2016
RETURN FREQUENCY: 1000-YEAR, 24 HR
ABSTRACTION TECHNIQUE: SCS CURVE NUMBER

```

Appendix III-1  
Page 5 of 24

```

SCENARIO: UPPER POND A FLOWING INTO SECTIONS D AND E
.....
14 IO OUTPUT CONTROL VARIABLES
      IPRINT 4 PRINT CONTROL
      I PLOT 0 PLOT CONTROL
      OSCAL 0 HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA
      NMN 1 MINUTES IN COMPUTATION INTERVAL
      I DATE 1 0 STARTING DATE
      I TIME 0000 STARTING TIME
      NO 1440 NUMBER OF HYDROGRAPH ORDINATES
      NDDATE 1 0 ENDING DATE
      NDTIME 2359 ENDING TIME
      I CENT 19 CENTURY MARK

COMPUTATION INTERVAL 02 HOURS
TOTAL TIME BASE 23.98 HOURS

ENGLISH UNITS
DRAINAGE AREA SQUARE MILES
PRECIPITATION DEPTH INCHES
LENGTH, ELEVATION FEET
FLOW CUBIC FEET PER SECOND
STORAGE VOLUME ACRES- FEET
SURFACE AREA ACRES
TEMPERATURE DEGREES FAHRENHEIT

JP MULTI-PLAN OPTION
NPLAN 1 NUMBER OF PLANS

JR MULTI-RATIO OPTION
RATIOS OF PRECIPITATION
13.60

```

```

*****
* UPA *

```

Appendix III-1  
Page 6 of 24

```

*****
COAL PILE AND UPPER POND A
13 IN TIME DATA FOR INPUT TIME SERIES
      JXMIN 72 TIME INTERVAL IN MINUTES
      JXDATE 1 0 STARTING DATE
      JXTIME 0 STARTING TIME

SUBBASIN RUNOFF DATA
19 BA SUBBASIN CHARACTERISTICS
      TAREA .04 SUBBASIN AREA

PRECIPITATION DATA
19 PB STORM 1.00 BASIN TOTAL PRECIPITATION

19 PI INCREMENTAL PRECIPITATION PATTERN
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00

```

Appendix III-1  
Page 7 of 24

```

      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00
      .00 .00 .00 .00 .00 .00 .00 .00 .00

```

Appendix III-1  
Page 8 of 24

Table with 10 columns of numerical data, mostly zeros, representing model output for Appendix III-1.

Table with 10 columns of numerical data, including labels like 'SCS LOSS RATE', 'SCS DIMENSIONLESS UNIT GRAPH', and 'UNIT HYDROGRAPH'. Includes values like 0.04, 98.00, 0.05, 17, 55, 189, 301, 301, 234, 140, 87, 56, 35, 22.

Table with 4 columns: ID, STORAGE ROUTING, ELEVATION, and INITIAL CONDITION. Includes sections for 'UPPER POND A', 'HYDROGRAPH ROUTING DATA', and 'COMPUTED STORAGE-ELEVATION DATA'.

Table with 10 columns of numerical data, including labels like 'SECTION D', 'SUBBASIN RUNOFF DATA', 'SUBBASIN CHARACTERISTICS', 'PRECIPITATION DATA', and 'INCREMENTAL PRECIPITATION PATTERN'.

Table with 10 columns of numerical data, mostly zeros, representing model output for Section D and Section E.

Table with 10 columns of numerical data, mostly zeros, representing model output for Section D and Section E.

Table with 10 columns of numerical data, mostly zeros, representing model output for Section D and Section E.

58 LS SCS LOSS RATE STRL 04 INITIAL ABSTRACTION CRVNR 98.00 CURVE NUMBER RTIMP .00 PERCENT IMPERVIOUS AREA

59 UD SCS DIMENSIONLESS UNIT GRAPH TLAG .05 LAG

UNI T HYDROGRAPH 17 END-OF-PERIOD ORDINATES

15. 51. 82. 82. 64. 38. 24. 15. 10. 6. 4. 2. 1. 1. 1. 0. 0.

60 KK \*\*\*\*\* COMB \*\*\*\*\* KK

62 HC HYDROGRAPH COMBINATION ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE \*\*\*

63 KK \*\*\*\*\* BASND \*\*\*\*\*

65 RS STORAGE ROUTING NSTPS 1 NUMBER OF SUBREACHES I TYP ELEV TYPE OF INITIAL CONDITION RSVRI C 947.00 INITIAL CONDITION X .00 WORKING R AND D COEFFICIENT

66 SA AREA .7 1.9 4.2 4.8 5.0 5.2

67 SE ELEVATION 947.00 948.00 949.00 950.00 951.00 952.00

68 SQ DISCHARGE 0. 0. 10. 10. 10. 12.

69 SE ELEVATION 947.00 948.00 949.00 950.00 951.00 952.00

COMPUTED STORAGE-ELEVATION DATA



75 UD SCS DIMENSIONLESS UNIT GRAPH  
TLAG .05 LAG  
\*\*\*  
UNIT HYDROGRAPH  
17 END-OF-PERIOD ORDINATES  
16. 55. 88. 88. 17. 10. 6.  
4. 3. 2. 1. 1. 0. 0.

\*\*\*\*\*  
\* \* \*  
\* COMB \*  
\* \* \*  
\*\*\*\*\*  
COMBINATION OF SUB BASINS KM

78 HC HYDROGRAPH COMBINATION  
ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE  
\*\*\*

\*\*\*\*\*  
\* \* \*  
\* BASNE \*  
\* \* \*  
\*\*\*\*\*  
BASIN IN SECTION E

HYDROGRAPH ROUTING DATA  
81 RS STORAGE ROUTING  
NSTPS 1 NUMBER OF SUBREACHES  
ITYP ELEV TYPE OF INITIAL CONDITION

Appendix III-1  
Page 21 of 24

+ UPA .04 1 FLOW TIME 14. 23.98  
\*\* PEAK STAGES IN FEET \*\*  
1 STAGE 953.45  
TIME 23.98  
HYDROGRAPH AT  
+ SECD .01 1 FLOW TIME 4. 18.27  
2 COMBINED AT  
+ COMB .05 1 FLOW TIME 18. 23.98  
ROUTED TO  
+ BASND .05 1 FLOW TIME 11. 23.98  
\*\* PEAK STAGES IN FEET \*\*  
1 STAGE 951.41  
TIME 23.98  
HYDROGRAPH AT  
+ SECE .01 1 FLOW TIME 4. 18.27  
2 COMBINED AT  
+ COMB .06 1 FLOW TIME 15. 23.98  
ROUTED TO  
+ BASNE .06 1 FLOW TIME 0. .00  
\*\* PEAK STAGES IN FEET \*\*  
1 STAGE 946.61  
TIME 23.98

\*\*\* NORMAL END OF HEC-1 \*\*\*

Appendix III-1  
Page 23 of 24

|       | RSVRI C X | 939.00 | INITIAL CONDITION | WORKING R AND D | COEFFICIENT |        |        |        |        |        |        |
|-------|-----------|--------|-------------------|-----------------|-------------|--------|--------|--------|--------|--------|--------|
| 82 SA | AREA      | .1     | .4                | .8              | 2.2         | 4.4    | 5.3    | 5.5    | 5.6    | 5.8    | 6.0    |
| 83 SE | ELEVATION | 939.00 | 940.00            | 941.00          | 942.00      | 943.00 | 944.00 | 945.00 | 946.00 | 947.00 | 948.00 |
| 84 SQ | DISCHARGE | 0.     | 0.                | 0.              | 0.          | 0.     | 0.     | 0.     | 0.     | 0.     | 0.     |
| 85 SE | ELEVATION | 939.00 | 940.00            | 941.00          | 942.00      | 943.00 | 944.00 | 945.00 | 946.00 | 947.00 | 948.00 |

\*\*\*  
COMPUTED STORAGE-ELEVATION DATA  
STORAGE .00 .21 .79 2.24 5.48 10.33 15.70 21.27 27.00 32.90  
ELEVATION 939.00 940.00 941.00 942.00 943.00 944.00 945.00 946.00 947.00 948.00

COMPUTED STORAGE-OUTFLOW-ELEVATION DATA  
STORAGE .00 .21 .79 2.24 5.48 10.33 15.70 21.27 27.00 32.90  
OUTFLOW .00 .00 .00 .00 .00 .00 .00 .00 .00 .00  
ELEVATION 939.00 940.00 941.00 942.00 943.00 944.00 945.00 946.00 947.00 948.00

1

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS  
FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES  
TIME TO PEAK IN HOURS

| OPERATION     | STATION | AREA | PLAN | RATIO 1 | RATIOS APPLIED TO PRECIPITATION |
|---------------|---------|------|------|---------|---------------------------------|
|               |         |      |      | 13.60   |                                 |
| HYDROGRAPH AT | UPA     | .04  | 1    | 15.     |                                 |
| ROUTED TO     |         |      |      | 21.22   |                                 |

Appendix III-1  
Page 22 of 24

Appendix III-1  
Page 24 of 24





**APPENDIX III-2**  
**HEC-1 OUTPUT**  
**LOWER POND C**

FLOOD HYDROGRAPH PACKAGE (HEC-1)
JUN 1998
VERSION 4.1
RUN DATE 05OCT16 TIME 15:36:58
U.S. ARMY CORPS OF ENGINEERS
HYDROLOGIC ENGINEERING CENTER
609 SECOND STREET
DAVIS, CALIFORNIA 95616
(916) 756-1104

X X XXXXXX XXXX X
X X X X X XX
X X X X X X
XXXXXX XXXX X XXXX X
X X X X X X
X X XXXXXX XXXX XXX

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.
THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTI OR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.
THE DEFINITION OF -MSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION
NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,
DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL, LOSS RATE:GREEN AND AMPT INFILTRATION
KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1 HEC-1 INPUT PAGE 1
LINE ID 1 2 3 4 5 6 7 8 9 10
1 ID
2 ID PROJECT NAME: EDE ASBURY
3 ID CONSULTANT: PALMERTON & PARRISH, INC.
4 ID PROJECT NUMBER: 231518
5 ID DESIGN ENGINEER: DONALD C. NOWACK, P. E.
6 ID FILE NAME: C.TXT

Appendix III-2
Page 1 of 11

35 PC 0.8535 0.8565 0.8594 0.8622 0.8649 0.8676 0.8702 0.8728 0.8753 0.8777
36 PC 0.8800 0.8823 0.8845 0.8868 0.8890 0.8912 0.8934 0.8955 0.8976 0.8997
37 PC 0.9018 0.9038 0.9058 0.9078 0.9097 0.9117 0.9136 0.9155 0.9173 0.9192
38 PC 0.9210 0.9228 0.9245 0.9263 0.9280 0.9297 0.9313 0.9330 0.9346 0.9362
39 PC 0.9377 0.9393 0.9408 0.9423 0.9438 0.9452 0.9466 0.9480 0.9493 0.9507

HEC-1 INPUT PAGE 2
LINE ID 1 2 3 4 5 6 7 8 9 10
40 PC 0.9520 0.9533 0.9546 0.9559 0.9572 0.9584 0.9597 0.9610 0.9622 0.9635
41 PC 0.9647 0.9660 0.9672 0.9685 0.9697 0.9709 0.9722 0.9734 0.9746 0.9758
42 PC 0.9770 0.9782 0.9794 0.9806 0.9818 0.9829 0.9841 0.9853 0.9864 0.9876
43 PC 0.9887 0.9899 0.9910 0.9922 0.9933 0.9944 0.9956 0.9967 0.9978 0.9989
44 PC 1.0000
\* SCS CURVE NUMBER: 98.00
LS 98.00
\* TIME OF CONCENTRATION: 0.0833 HR (LAG TIME = 0.6 \* Tc = 0.0500 HR)
UD 0.0500
47 KK BASNC
48 KM BASINC
49 RS 1 ELEV 950.0
50 SA 0.5564 5.4486 9.2805 10.598 11.433 11.769
51 SE 950.0 0.951 0.952 0.953 0.954 0.955 0
52 SO 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000
53 SE 950.0 0.951 0.952 0.953 0.954 0.955 0

54 ZZ
SCHEMATIC DIAGRAM OF STREAM NETWORK
INPUT LINE (V) ROUTING (--->) DIVERSION OR PUMP FLOW
NO. (.) CONNECTOR (<---) RETURN OF DIVERTED OR PUMPED FLOW
16 SUBAC
V
47 BASNC

(\*\*\*) RUNOFF ALSO COMPUTED AT THIS LOCATION

Appendix III-2
Page 3 of 11

ID DATE: OCTOBER 17, 2016
ID RETURN FREQUENCY: 1000-YEAR, 24 HR
ID ABSTRACTION TECHNIQUE: SCS CURVE NUMBER
ID SCENARIO: AREA C
NUMBER OF 1 MIN INTERVALS USED FOR CALCULATION
\*\*\*No OF INTERVALS\*\*1-060 2-120 3-180 6-360 12-720 18-1080 24-1440
NUMBER OF MIN IN EACH TIME INTERVAL
\*\*\*MIN IN INTERVAL\*\*1hr-3 2hr-6 3hr-9 6hr-18 12hr-36 18-54 24-72
IN 72
IO 4
DI AGRAM 0
\* 1000-YR
JR PREC 13.60
\* STORM DISTRIBUTION: SCS TYPE II
\* STORM DURATION: 24 HOUR
\* 1 2 3 4 5 6 7 8 9 10
KK SUBAC
KM SUB AREA C
PB 1.00
\* DRAINAGE AREA: 12.40 ACRES = 0.0194 SQ. MI.
RA 0.0194
\* RAINFALL DISTRIBUTION
PC 0.0000 0.0010 0.0020 0.0030 0.0041 0.0051 0.0062 0.0072 0.0083 0.0094
PC 0.0105 0.0116 0.0127 0.0138 0.0150 0.0161 0.0173 0.0184 0.0196 0.0208
PC 0.0220 0.0232 0.0244 0.0257 0.0269 0.0281 0.0294 0.0306 0.0319 0.0332
PC 0.0345 0.0358 0.0371 0.0384 0.0398 0.0411 0.0425 0.0439 0.0452 0.0466
PC 0.0480 0.0494 0.0508 0.0523 0.0538 0.0553 0.0568 0.0583 0.0598 0.0614
PC 0.0630 0.0646 0.0662 0.0679 0.0696 0.0712 0.0730 0.0747 0.0764 0.0782
PC 0.0800 0.0818 0.0836 0.0855 0.0874 0.0892 0.0912 0.0931 0.0950 0.0970
PC 0.0990 0.1010 0.1030 0.1051 0.1072 0.1093 0.1114 0.1135 0.1156 0.1178
PC 0.1200 0.1222 0.1246 0.1270 0.1296 0.1322 0.1350 0.1379 0.1408 0.1438
PC 0.1470 0.1502 0.1534 0.1566 0.1598 0.1630 0.1663 0.1697 0.1733 0.1771
PC 0.1810 0.1851 0.1895 0.1941 0.1989 0.2040 0.2094 0.2152 0.2214 0.2280
PC 0.2350 0.2427 0.2513 0.2609 0.2715 0.2830 0.3068 0.3544 0.4308 0.5679
PC 0.6630 0.6820 0.6986 0.7130 0.7252 0.7350 0.7434 0.7514 0.7588 0.7656
PC 0.7720 0.7780 0.7835 0.7890 0.7942 0.7990 0.8036 0.8080 0.8122 0.8162
PC 0.8200 0.8237 0.8273 0.8308 0.8342 0.8375 0.8409 0.8442 0.8474 0.8505

Appendix III-2
Page 2 of 11

FLOOD HYDROGRAPH PACKAGE (HEC-1)
JUN 1998
VERSION 4.1
RUN DATE 05OCT16 TIME 15:36:58
U.S. ARMY CORPS OF ENGINEERS
HYDROLOGIC ENGINEERING CENTER
609 SECOND STREET
DAVIS, CALIFORNIA 95616
(916) 756-1104

PROJECT NAME: EDE ASBURY
CONSULTANT: PALMERTON & PARRISH, INC.
PROJECT NUMBER: 231518
DESIGN ENGINEER: DONALD C. NOWACK, P. E.
FILE NAME: C.TXT
DATE: OCTOBER 17, 2016
RETURN FREQUENCY: 1000-YEAR, 24 HR
ABSTRACTION TECHNIQUE: SCS CURVE NUMBER
SCENARIO: AREA C

14 10 OUTPUT CONTROL VARIABLES
I PRINT 4 PRINT CONTROL
I PLOT 0 PLOT CONTROL
OSCAL 0 HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA
MIN 1 MINUTES IN COMPUTATION INTERVAL
IDATE 1 0 STARTING DATE
ITIME 0000 STARTING TIME
NQ 1440 NUMBER OF HYDROGRAPH ORDINATES
NDDATE 1 0 ENDING DATE
NDTIME 2359 ENDING TIME
ICENT 19 CENTURY MARK
COMPUTATION INTERVAL 02 HOURS
TOTAL TIME BASE 23.98 HOURS

ENGLISH UNITS
DRAINAGE AREA SQUARE MILES
PRECIPITATION DEPTH INCHES

Appendix III-2
Page 4 of 11



```

.00 .00 .00 .00 .00 .00 .00 .00 .00 .00
.00 .00 .00 .00 .00 .00 .00 .00 .00 .00
.00 .00 .00 .00 .00 .00 .00 .00 .00 .00
.00 .00 .00 .00 .00 .00 .00 .00 .00 .00
.00 .00 .00 .00 .00 .00 .00 .00 .00 .00
.00 .00 .00 .00 .00 .00 .00 .00 .00 .00
.00 .00 .00 .00 .00 .00 .00 .00 .00 .00
.00 .00 .00 .00 .00 .00 .00 .00 .00 .00
.00 .00 .00 .00 .00 .00 .00 .00 .00 .00
45 LS  SCS LOSS RATE          .04  I N I T I A L A B S T R A C T I O N
      STRTL                98.00  C U R V E  N U M B E R
      CRVNR                .00    P E R C E N T  I M P E R V I O U S  A R E A
      RTIMP
46 UD  SCS DIMENSIONLESS UNI T G R A P H
      TLAG                .05  L A G
***
UNI T  H Y D R O G R A P H
17  E N D - O F - P E R I O D  O R D I N A T E S
28.  97.  155.  155.  121.  72.  45.  29.  18.  11.
7.   4.   3.   2.   1.   1.   0.

```

```

*****
*          *
*  BASNC  *
*          *
*****
      BASIN C
HYDROGRAPH ROUTING DATA
49 RS  STORAGE ROUTING
      NSTPS                1  N U M B E R  O F  S U B R E A C H E S
      ITYP                 ELEV  T Y P E  O F  I N I T I A L  C O N D I T I O N
      RSVR C              950.00  I N I T I A L  C O N D I T I O N
      X                    .00  W O R K I N G  R  A N D  D  C O E F F I C I E N T

```

|       |           |        |        |        |        |        |        |
|-------|-----------|--------|--------|--------|--------|--------|--------|
| 50 SA | AREA      | .6     | 5.4    | 9.3    | 10.6   | 11.4   | 11.8   |
| 51 SE | ELEVATION | 950.00 | 951.00 | 952.00 | 953.00 | 954.00 | 955.00 |
| 52 SQ | DISCHARGE | 0.     | 0.     | 0.     | 0.     | 0.     | 0.     |
| 53 SE | ELEVATION | 950.00 | 951.00 | 952.00 | 953.00 | 954.00 | 955.00 |

\*\*\*

| COMPUTED STORAGE-ELEVATION DATA |  |        |        |        |        |        |        |
|---------------------------------|--|--------|--------|--------|--------|--------|--------|
| STORAGE                         |  | .00    | 2.58   | 9.86   | 19.79  | 30.81  | 42.41  |
| ELEVATION                       |  | 950.00 | 951.00 | 952.00 | 953.00 | 954.00 | 955.00 |

| COMPUTED STORAGE-OUTFLOW-ELEVATION DATA |  |        |        |        |        |        |        |
|---|--|--------|--------|--------|--------|--------|--------|
| STORAGE                                 |  | .00    | 2.58   | 9.86   | 19.79  | 30.81  | 42.41  |
| OUTFLOW                                 |  | .00    | .00    | .00    | .00    | .00    | .00    |
| ELEVATION                               |  | 950.00 | 951.00 | 952.00 | 953.00 | 954.00 | 955.00 |

1 PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS  
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES  
 TIME TO PEAK IN HOURS

| OPERATION     | STATION | AREA | PLAN | RATIO | RATIOS APPLIED TO PRECIPITATION |        |
|---------------|---------|------|------|-------|---------------------------------|--------|
|               |         |      |      | 1     | 13.60                           |        |
| HYDROGRAPH AT |         |      |      |       |                                 |        |
| +             | SUBAC   | .02  | 1    | FLOW  | 8.                              |        |
|               |         |      |      | TIME  | 21.87                           |        |
| ROUTED TO     |         |      |      |       |                                 |        |
| +             | BASNC   | .02  | 1    | FLOW  | 0.                              |        |
|               |         |      |      | TIME  | .00                             |        |
|               |         |      |      | **    | PEAK STAGES IN FEET **          |        |
|               |         |      |      | 1     | STAGE                           | 952.39 |
|               |         |      |      |       | TIME                            | 23.98  |

\*\*\* NORMAL END OF HEC-1 \*\*\*



**APPENDIX III-3**  
**HEC-1 OUTPUT**  
**SECTION F**

FLOOD HYDROGRAPH PACKAGE (HEC-1)
JUN 1998
VERSION 4.1
RUN DATE 11OCT16 TIME 14:18:37
U.S. ARMY CORPS OF ENGINEERS
HYDROLOGIC ENGINEERING CENTER
609 SECOND STREET
DAVIS, CALIFORNIA 95616
(916) 756-1104

X X XXXXXX XXXX X
X X X X X XX
X X X X X X
XXXXXX XXXX X XXXX X
X X X X X X
X X XXXXXX XXXX XXX

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTI OR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.
THE DEFINITION OF -MSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION
NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,
DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL, LOSS RATE:GREEN AND AMPT INFILTRATION
KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1 HEC-1 INPUT PAGE 1
LINE ID 1 2 3 4 5 6 7 8 9 10
1 ID
2 ID PROJECT NAME: EDE ASBURY
3 ID CONSULTANT: PALMERTON & PARRISH, INC.
4 ID PROJECT NUMBER: 231518
5 ID DESIGN ENGINEER: DONALD C. NOWACK, P. E.
6 ID FILE NAME: F.TXT

Appendix III-3
Page 1 of 11

35 PC 0.8535 0.8565 0.8594 0.8622 0.8649 0.8676 0.8702 0.8728 0.8753 0.8777
36 PC 0.8800 0.8823 0.8845 0.8868 0.8890 0.8912 0.8934 0.8955 0.8976 0.8997
37 PC 0.9018 0.9038 0.9058 0.9078 0.9097 0.9117 0.9136 0.9155 0.9173 0.9192
38 PC 0.9210 0.9228 0.9245 0.9263 0.9280 0.9297 0.9313 0.9330 0.9346 0.9362
39 PC 0.9377 0.9393 0.9408 0.9423 0.9438 0.9452 0.9466 0.9480 0.9493 0.9507
HEC-1 INPUT PAGE 2

LINE ID 1 2 3 4 5 6 7 8 9 10
40 PC 0.9520 0.9533 0.9546 0.9559 0.9572 0.9584 0.9597 0.9610 0.9622 0.9635
41 PC 0.9647 0.9660 0.9672 0.9685 0.9697 0.9709 0.9722 0.9734 0.9746 0.9758
42 PC 0.9770 0.9782 0.9794 0.9806 0.9818 0.9829 0.9841 0.9853 0.9864 0.9876
43 PC 0.9887 0.9899 0.9910 0.9922 0.9933 0.9944 0.9956 0.9967 0.9978 0.9989
44 PC 1.0000
\* SCS CURVE NUMBER: 98.00
45 LS 98.00
\* TIME OF CONCENTRATION: 0.0833 HR (LAG TIME = 0.6 \* Tc = 0.0500 HR)
46 UD 0.0500
47 KK BASNF
48 KM BASIN SECTION F
49 RS 1 ELEV 946.0
50 SA 0.0814 0.3307 0.6452 1.5414 1.8699 2.3758 3.1287 3.3812
51 SE 946.0 0.947.0 948.0 949.0 950.0 951.0 952.0 953.0
52 SO 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000
53 SE 946.0 0.947.0 948.0 949.0 950.0 951.0 952.0 953.0
\* 1 2 3 4 5 6 7 8 9 10
54 ZZ

INPUT LINE (V) ROUTING (--->) DIVERSION OR PUMP FLOW
NO. (.) CONNECTOR (<---) RETURN OF DIVERTED OR PUMPED FLOW
16 SECF
V
47 BASNF

(\*\*\*) RUNOFF ALSO COMPUTED AT THIS LOCATION

Appendix III-3
Page 3 of 11

ID DATE: OCTOBER 17, 2016
ID RETURN FREQUENCY: 1000-YEAR, 24 HR
ID ABSTRACTION TECHNIQUE: SCS CURVE NUMBER
ID SCENARIO: SECTION F
NUMBER OF 1 MIN INTERVALS USED FOR CALCULATION
\*\*\*No Of INTERVALS\*\*\*1-060 2-120 3-180 6-360 12-720 18-1080 24-1440
NUMBER OF MIN IN EACH TIME INTERVAL
\*\*\*MIN IN INTERVAL\*\*\*1hr-3 2hr-6 3hr-9 6hr-18 12hr-36 18-54 24-72
IN 72
IO 4 0
DI AGRAM
1000-YR
JR PREC 13.60
SCS TYPE II
STORM DURATION: 24 HOUR
1 2 3 4 5 6 7 8 9 10
KK SECF
KM SECTION F
PB 1.00
DRAINAGE AREA: 3.99 ACRES = 0.0062 SQ. MI.
BA 0.0062
RAINFALL DISTRIBUTION
PC 0.0000 0.0010 0.0020 0.0030 0.0041 0.0051 0.0062 0.0072 0.0083 0.0094
PC 0.0105 0.0116 0.0127 0.0138 0.0150 0.0161 0.0173 0.0184 0.0196 0.0208
PC 0.0220 0.0232 0.0244 0.0257 0.0269 0.0281 0.0294 0.0306 0.0319 0.0332
PC 0.0345 0.0358 0.0371 0.0384 0.0398 0.0411 0.0425 0.0439 0.0452 0.0466
PC 0.0480 0.0494 0.0508 0.0523 0.0538 0.0553 0.0568 0.0583 0.0598 0.0614
PC 0.0630 0.0646 0.0662 0.0679 0.0696 0.0712 0.0730 0.0747 0.0764 0.0782
PC 0.0800 0.0818 0.0836 0.0855 0.0874 0.0892 0.0912 0.0931 0.0950 0.0970
PC 0.0990 0.1010 0.1030 0.1051 0.1072 0.1093 0.1114 0.1135 0.1156 0.1178
PC 0.1200 0.1222 0.1246 0.1270 0.1296 0.1322 0.1350 0.1379 0.1408 0.1438
PC 0.1470 0.1502 0.1534 0.1566 0.1598 0.1630 0.1663 0.1697 0.1733 0.1771
PC 0.1810 0.1851 0.1895 0.1941 0.1989 0.2040 0.2094 0.2152 0.2214 0.2280
PC 0.2350 0.2427 0.2513 0.2609 0.2715 0.2830 0.3068 0.3544 0.4308 0.5679
PC 0.6630 0.6820 0.6986 0.7130 0.7252 0.7350 0.7434 0.7514 0.7588 0.7656
PC 0.7720 0.7780 0.7835 0.7890 0.7942 0.7990 0.8036 0.8080 0.8122 0.8162
PC 0.8200 0.8237 0.8273 0.8308 0.8342 0.8375 0.8409 0.8442 0.8474 0.8505

Appendix III-3
Page 2 of 11

FLOOD HYDROGRAPH PACKAGE (HEC-1)
JUN 1998
VERSION 4.1
RUN DATE 11OCT16 TIME 14:18:37
U.S. ARMY CORPS OF ENGINEERS
HYDROLOGIC ENGINEERING CENTER
609 SECOND STREET
DAVIS, CALIFORNIA 95616
(916) 756-1104

PROJECT NAME: EDE ASBURY
CONSULTANT: PALMERTON & PARRISH, INC.
PROJECT NUMBER: 231518
DESIGN ENGINEER: DONALD C. NOWACK, P. E.
FILE NAME: F.TXT
DATE: OCTOBER 17, 2016
RETURN FREQUENCY: 1000-YEAR, 24 HR
ABSTRACTION TECHNIQUE: SCS CURVE NUMBER
SCENARIO: SECTION F

OUTPUT CONTROL VARIABLES
IPRINT 4 PRINT CONTROL
IPL0T 0 PLOT CONTROL
OSCAL 0 HYDROGRAPH PLOT SCALE

HYDROGRAPH TIME DATA
MIN 1 MINUTES IN COMPUTATION INTERVAL
IDATE 1 0 STARTING DATE
ITIME 0000 STARTING TIME
NQ 1440 NUMBER OF HYDROGRAPH ORDINATES
NDDATE 1 0 ENDING DATE
NDTIME 2359 ENDING TIME
ICENT 19 CENTURY MARK
COMPUTATION INTERVAL 02 HOURS
TOTAL TIME BASE 23.98 HOURS

ENGLISH UNITS
DRAINAGE AREA SQUARE MILES
PRECIPITATION DEPTH INCHES

Appendix III-3
Page 4 of 11





|     |     |     |     |     |     |     |     |     |     |     |     |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 |
| .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 |
| .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 |
| .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 |
| .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 |
| .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 |
| .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 |
| .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 |
| .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 |
| .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 | .00 |

45 LS     SCS LOSS RATE  
 STRL     .04     I N I T I A L   A B S T R A C T I O N  
 CRVNR    98.00    C U R V E   N U M B E R  
 RTIMP    .00     P E R C E N T   I M P E R V I O U S   A R E A

46 UD     SCS DIMENSIONLESS UNIT GRAPH  
 TLAG     .05     L A G

\*\*\*

U N I T   H Y D R O G R A P H  
 17 E N D - O F - P E R I O D   O R D I N A T E S

|    |     |     |     |     |     |     |    |    |    |
|----|-----|-----|-----|-----|-----|-----|----|----|----|
| 9. | 31. | 50. | 50. | 39. | 23. | 14. | 9. | 6. | 4. |
| 2. | 1.  | 1.  | 1.  | 0.  | 0.  | 0.  |    |    |    |

```

*****
*                                     *
*    BASNF                            *
*    *                                     *
*    *                                     *
*****
    BASIN SECTION F
HYDROGRAPH ROUTING DATA
49 RS     STORAGE ROUTING
         NSTPS    1    N U M B E R   O F   S U B R E A C H E S
         ITYP    ELEV    T Y P E   O F   I N I T I A L   C O N D I T I O N
         RSVR C    946.00    I N I T I A L   C O N D I T I O N
         X            .00    W O R K I N G   R   A N D   D   C O E F F I C I E N T
    
```

\*\*\* NORMAL END OF HEC-1 \*\*\*

|       |           |        |        |        |        |        |        |        |        |
|-------|-----------|--------|--------|--------|--------|--------|--------|--------|--------|
| 50 SA | AREA      | .1     | .3     | .6     | 1.5    | 1.9    | 2.4    | 3.1    | 3.4    |
| 51 SE | ELEVATION | 946.00 | 947.00 | 948.00 | 949.00 | 950.00 | 951.00 | 952.00 | 953.00 |
| 52 SQ | DISCHARGE | 0.     | 0.     | 0.     | 0.     | 0.     | 0.     | 0.     | 0.     |
| 53 SE | ELEVATION | 946.00 | 947.00 | 948.00 | 949.00 | 950.00 | 951.00 | 952.00 | 953.00 |

\*\*\*

COMPUTED STORAGE-ELEVATION DATA

|           |        |        |        |        |        |        |        |        |
|-----------|--------|--------|--------|--------|--------|--------|--------|--------|
| STORAGE   | .00    | .19    | .67    | 1.73   | 3.44   | 5.55   | 8.30   | 11.55  |
| ELEVATION | 946.00 | 947.00 | 948.00 | 949.00 | 950.00 | 951.00 | 952.00 | 953.00 |

COMPUTED STORAGE-OUTFLOW-ELEVATION DATA

|           |        |        |        |        |        |        |        |        |
|-----------|--------|--------|--------|--------|--------|--------|--------|--------|
| STORAGE   | .00    | .19    | .67    | 1.73   | 3.44   | 5.55   | 8.30   | 11.55  |
| OUTFLOW   | .00    | .00    | .00    | .00    | .00    | .00    | .00    | .00    |
| ELEVATION | 946.00 | 947.00 | 948.00 | 949.00 | 950.00 | 951.00 | 952.00 | 953.00 |

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS  
 FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES  
 TIME TO PEAK IN HOURS

| OPERATION     | STATION | AREA | PLAN                      | RATIO  |
|---------------|---------|------|---------------------------|--------|
|               |         |      |                           | 1      |
|               |         |      |                           | 13.60  |
| HYDROGRAPH AT |         |      |                           |        |
| +             | SECF    | .01  | 1                         | 2.     |
|               |         |      | FLOW                      | 18.37  |
|               |         |      | TIME                      |        |
| ROUTED TO     |         |      |                           |        |
| +             | BASNF   | .01  | 1                         | 0.     |
|               |         |      | FLOW                      | .00    |
|               |         |      | TIME                      |        |
|               |         |      | ** PEAK STAGES IN FEET ** |        |
|               |         |      | 1                         | 950.46 |
|               |         |      | STAGE                     | 23.98  |
|               |         |      | TIME                      |        |



**APPENDIX III-4**  
**HEC-1 OUTPUT**  
**SECTION G**

FLOOD HYDROGRAPH PACKAGE (HEC-1)
JUN 1998
VERSION 4.1
RUN DATE 11OCT16 TIME 14:18:47
U.S. ARMY CORPS OF ENGINEERS
HYDROLOGIC ENGINEERING CENTER
609 SECOND STREET
DAVIS, CALIFORNIA 95616
(916) 756-1104

X X XXXXXX XXXX X
X X X X X XX
X X X X X X
XXXXXX XXXX X XXXX X
X X X X X X
X X XXXXXX XXXX XXX

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.
THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTI OR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.
THE DEFINITION OF -MSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION
NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,
DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION
KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

HEC-1 INPUT PAGE 1
LINE ID 1 2 3 4 5 6 7 8 9 10
1 ID
2 ID PROJECT NAME: EDE ASBURY
3 ID CONSULTANT: PALMERTON & PARRISH, INC.
4 ID PROJECT NUMBER: 231518
5 ID DESIGN ENGINEER: DONALD C. NOWACK, P. E.
6 ID FILE NAME: G.TXT
Appendix III-4
Page 1 of 11

PC 0.8535 0.8565 0.8594 0.8622 0.8649 0.8676 0.8702 0.8728 0.8753 0.8777
PC 0.8800 0.8823 0.8845 0.8868 0.8890 0.8912 0.8934 0.8955 0.8976 0.8997
PC 0.9018 0.9038 0.9058 0.9078 0.9097 0.9117 0.9136 0.9155 0.9173 0.9192
PC 0.9210 0.9228 0.9245 0.9263 0.9280 0.9297 0.9313 0.9330 0.9346 0.9362
PC 0.9377 0.9393 0.9408 0.9423 0.9438 0.9452 0.9466 0.9480 0.9493 0.9507
HEC-1 INPUT PAGE 2
LINE ID 1 2 3 4 5 6 7 8 9 10
40 PC 0.9520 0.9533 0.9546 0.9559 0.9572 0.9584 0.9597 0.9610 0.9622 0.9635
41 PC 0.9647 0.9660 0.9672 0.9685 0.9697 0.9709 0.9722 0.9734 0.9746 0.9758
42 PC 0.9770 0.9782 0.9794 0.9806 0.9818 0.9829 0.9841 0.9853 0.9864 0.9876
43 PC 0.9887 0.9899 0.9910 0.9922 0.9933 0.9944 0.9956 0.9967 0.9978 0.9989
44 PC 1.0000
\* SCS CURVE NUMBER: 98.00
LS 98.00
\* TIME OF CONCENTRATION: 0.0833 HR (LAG TIME = 0.6 \* Tc = 0.0500 HR)
UD 0.0500
47 KK BASNG
48 KM BASIN SECTION G
49 RS 1 ELEV 937.0
50 SA 0.0631 0.6902 1.2727 1.5650 1.7619 1.8770 2.1662 2.3247 2.4937 2.6722
51 SE 937.0 938.0 939.0 940.0 941.0 942.0 943.0 944.0 945.0 946.0
52 SO 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000
53 SE 937.0 938.0 939.0 940.0 941.0 942.0 943.0 944.0 945.0 946.0
\* 1 2 3 4 5 6 7 8 9 10
ZZ

SCHEMATIC DIAGRAM OF STREAM NETWORK
INPUT LINE (V) ROUTING (--->) DIVERSION OR PUMP FLOW
NO. (.) CONNECTOR (<---) RETURN OF DIVERTED OR PUMPED FLOW
16 SECG
V
47 BASNG

(\*\*\*) RUNOFF ALSO COMPUTED AT THIS LOCATION

ID DATE: OCTOBER 17, 2016
ID RETURN FREQUENCY: 1000-YEAR, 24 HR
ID ABSTRACTION TECHNIQUE: SCS CURVE NUMBER
ID SCENARIO: SECTION G
NUMBER OF 1 MIN INTERVALS USED FOR CALCULATION
\*\*\*No Of INTERVALS\*\*\*1-060 2-120 3-180 6-360 12-720 18-1080 24-1440
NUMBER OF MIN IN EACH TIME INTERVAL
\*\*\*MIN IN INTERVAL\*\*\*1hr-3 2hr-6 3hr-9 6hr-18 12hr-36 18-54 24-72
IN 72
IO 4
\*DIAGRAM
\* 1000-YR
JR PREC 13.60
\* STORM DISTRIBUTION: SCS TYPE II
\* STORM DURATION: 24 HOUR
\* 1 2 3 4 5 6 7 8 9 10
KK SECG
KM SECTION G
PB 1.00
\* DRAINAGE AREA: 4.39 ACRES = 0.0069 SQ. MI.
BA 0.0069
\* RAINFALL DISTRIBUTION
PC 0.0000 0.0010 0.0020 0.0030 0.0041 0.0051 0.0062 0.0072 0.0083 0.0094
PC 0.0105 0.0116 0.0127 0.0138 0.0150 0.0161 0.0173 0.0184 0.0196 0.0208
PC 0.0220 0.0232 0.0244 0.0257 0.0269 0.0281 0.0294 0.0306 0.0319 0.0332
PC 0.0345 0.0358 0.0371 0.0384 0.0398 0.0411 0.0425 0.0439 0.0452 0.0466
PC 0.0480 0.0494 0.0508 0.0523 0.0538 0.0553 0.0568 0.0583 0.0598 0.0614
PC 0.0630 0.0646 0.0662 0.0679 0.0696 0.0712 0.0730 0.0747 0.0764 0.0782
PC 0.0800 0.0818 0.0836 0.0855 0.0874 0.0892 0.0912 0.0931 0.0950 0.0970
PC 0.0990 0.1010 0.1030 0.1051 0.1072 0.1093 0.1114 0.1135 0.1156 0.1178
PC 0.1200 0.1222 0.1246 0.1270 0.1296 0.1322 0.1350 0.1379 0.1408 0.1438
PC 0.1470 0.1502 0.1534 0.1566 0.1598 0.1630 0.1663 0.1697 0.1733 0.1771
PC 0.1810 0.1851 0.1895 0.1941 0.1989 0.2040 0.2094 0.2152 0.2214 0.2280
PC 0.2350 0.2427 0.2513 0.2609 0.2715 0.2830 0.3068 0.3544 0.4308 0.5679
PC 0.6630 0.6820 0.6986 0.7130 0.7252 0.7350 0.7434 0.7514 0.7588 0.7656
PC 0.7720 0.7780 0.7835 0.7890 0.7942 0.7990 0.8036 0.8080 0.8122 0.8162
PC 0.8200 0.8237 0.8273 0.8308 0.8342 0.8375 0.8409 0.8442 0.8474 0.8505
Appendix III-4
Page 2 of 11

FLOOD HYDROGRAPH PACKAGE (HEC-1)
JUN 1998
VERSION 4.1
RUN DATE 11OCT16 TIME 14:18:47
U.S. ARMY CORPS OF ENGINEERS
HYDROLOGIC ENGINEERING CENTER
609 SECOND STREET
DAVIS, CALIFORNIA 95616
(916) 756-1104

PROJECT NAME: EDE ASBURY
CONSULTANT: PALMERTON & PARRISH, INC.
PROJECT NUMBER: 231518
DESIGN ENGINEER: DONALD C. NOWACK, P. E.
FILE NAME: G.TXT
DATE: OCTOBER 17, 2016
RETURN FREQUENCY: 1000-YEAR, 24 HR
ABSTRACTION TECHNIQUE: SCS CURVE NUMBER
SCENARIO: SECTION G

OUTPUT CONTROL VARIABLES
IPRINT 4 PRINT CONTROL
IPL0T 0 PLOT CONTROL
OSCAL 0 HYDROGRAPH PLOT SCALE

HYDROGRAPH TIME DATA
MIN 1 MINUTES IN COMPUTATION INTERVAL
IDATE 1 0 STARTING DATE
ITIME 0000 STARTING TIME
NQ 1440 NUMBER OF HYDROGRAPH ORDINATES
NDDATE 1 0 ENDING DATE
NDTIME 2359 ENDING TIME
ICENT 19 CENTURY MARK

COMPUTATION INTERVAL 02 HOURS
TOTAL TIME BASE 23.98 HOURS

ENGLISH UNITS
DRAINAGE AREA SQUARE MILES
PRECIPITATION DEPTH INCHES

Table with columns for parameters like LENGTH, ELEVATION, FEET, FLOW, STORAGE VOLUME, SURFACE AREA, TEMPERATURE, MULTI-PLAN OPTION, MULTI-RATIO OPTION, RATIO OF PRECIPITATION, TIME DATA FOR INPUT TIME SERIES, SUBBASIN RUNOFF DATA, SUBBASIN CHARACTERISTICS, PRECIPITATION DATA, and INCREMENTAL PRECIPITATION PATTERN.

Table with 10 columns of numerical data representing model outputs for various parameters.

Table with 10 columns of numerical data representing model outputs for various parameters.

Table with 10 columns of numerical data representing model outputs for various parameters.

```

.00 .00 .00 .00 .00 .00 .00 .00 .00 .00
.00 .00 .00 .00 .00 .00 .00 .00 .00 .00
.00 .00 .00 .00 .00 .00 .00 .00 .00 .00
.00 .00 .00 .00 .00 .00 .00 .00 .00 .00
.00 .00 .00 .00 .00 .00 .00 .00 .00 .00
.00 .00 .00 .00 .00 .00 .00 .00 .00 .00
.00 .00 .00 .00 .00 .00 .00 .00 .00 .00
.00 .00 .00 .00 .00 .00 .00 .00 .00 .00
45 LS SCS LOSS RATE .04 INITIAL ABSTRACTION
STRTL .04 CURVE NUMBER
CRVNR 98.00 PERCENT IMPERVIOUS AREA
RTIMP .00
46 UD SCS DIMENSIONLESS UNITGRAPH
TLAG .05 LAG
***
UNIT HYDROGRAPH
17 END-OF-PERIOD ORDINATES
10. 35. 55. 55. 43. 26. 16. 10. 6. 4.
3. 2. 1. 1. 0. 0. 0.

```

```

*****
* BASNG *
*****
BASIN SECTION G
HYDROGRAPH ROUTING DATA
49 RS STORAGE ROUTING
NSTPS 1 NUMBER OF SUBREACHES
ITYP ELEV TYPE OF INITIAL CONDITION
RSVRC 937.00 INITIAL CONDITION
X .00 WORKING R AND D COEFFICIENT

```

```

** PEAK STAGES IN FEET **
1 STAGE 941.29
TIME 23.98

```

\*\*\* NORMAL END OF HEC-1 \*\*\*

| STATION | TYPE      | 1      | 7      | 13     | 16     | 18     | 19     | 22     | 23     | 25     | 27     |
|---------|-----------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 50 SA   | AREA      | .1     | .7     | 1.3    | 1.6    | 1.8    | 1.9    | 2.2    | 2.3    | 2.5    | 2.7    |
| 51 SE   | ELEVATION | 937.00 | 938.00 | 939.00 | 940.00 | 941.00 | 942.00 | 943.00 | 944.00 | 945.00 | 946.00 |
| 52 SQ   | DISCHARGE | 0.     | 0.     | 0.     | 0.     | 0.     | 0.     | 0.     | 0.     | 0.     | 0.     |
| 53 SE   | ELEVATION | 937.00 | 938.00 | 939.00 | 940.00 | 941.00 | 942.00 | 943.00 | 944.00 | 945.00 | 946.00 |

\*\*\*

COMPUTED STORAGE-ELEVATION DATA

| STORAGE ELEVATION | 1      | 7      | 13     | 16     | 18     | 19     | 22     | 23     | 25     | 27     |
|-------------------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| STORAGE           | .00    | .32    | 1.29   | 2.70   | 4.37   | 6.19   | 8.21   | 10.45  | 12.86  | 15.44  |
| ELEVATION         | 937.00 | 938.00 | 939.00 | 940.00 | 941.00 | 942.00 | 943.00 | 944.00 | 945.00 | 946.00 |

COMPUTED STORAGE-OUTFLOW-ELEVATION DATA

| STORAGE   | 1      | 7      | 13     | 16     | 18     | 19     | 22     | 23     | 25     | 27     |
|-----------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| STORAGE   | .00    | .32    | 1.29   | 2.70   | 4.37   | 6.19   | 8.21   | 10.45  | 12.86  | 15.44  |
| OUTFLOW   | .00    | .00    | .00    | .00    | .00    | .00    | .00    | .00    | .00    | .00    |
| ELEVATION | 937.00 | 938.00 | 939.00 | 940.00 | 941.00 | 942.00 | 943.00 | 944.00 | 945.00 | 946.00 |

1  
PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS  
FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES  
TIME TO PEAK IN HOURS

| OPERATION     | STATION | AREA | PLAN | RATIO | TIME TO PEAK |
|---------------|---------|------|------|-------|--------------|
| HYDROGRAPH AT | SECG    | .01  | 1    | 13.60 | 3.18.27      |
| ROUTED TO     | BASNG   | .01  | 1    | 0.00  |              |



**APPENDIX III-5**

**HEC-HMS OUTPUT**

**SECTION H, SECTION I, UPPER POND B, & LOWER POND J**

**Project:** Flow\_Model**Simulation Run:** Run 1**Simulation Start:** 31 December 1999, 24:00**Simulation End:** 1 January 2000, 24:00**HMS Version:** 4.8**Executed:** 15 October 2021, 18:35

## Global Parameter Summary - Subbasin

### Area (ft<sup>2</sup>)

| Element Name | Area (ft <sup>2</sup> ) |
|--------------|-------------------------|
| Section H    | 0.01                    |
| Section B    | 0.02                    |
| Section J    | 0.06                    |
| Section I    | 0.02                    |

### Downstream

| Element Name | Downstream  |
|--------------|-------------|
| Section H    | Reservoir H |
| Section B    | Reservoir B |
| Section J    | Reservoir J |
| Section I    | Reservoir I |

### Loss Rate: Scs

| Element Name | Percent Impervious Area | Curve Number |
|--------------|-------------------------|--------------|
| Section H    | 0                       | 98           |
| Section B    | 0                       | 98           |
| Section J    | 0                       | 82.31        |
| Section I    | 0                       | 98           |

### Transform: Scs

| Element Name | Lag | Unitgraph Type |
|--------------|-----|----------------|
| Section H    | 3   | Standard       |
| Section B    | 3   | Standard       |
| Section J    | 3   | Standard       |
| Section I    | 3   | Standard       |

## Global Results Summary

| Hydrologic Element | Drainage Area (MI <sup>2</sup> ) | Peak Discharge (CFS) | Time of Peak     | Volume (IN) |
|--------------------|----------------------------------|----------------------|------------------|-------------|
| Section H          | 0.01                             | 172.49               | 01Jan2000, 11:56 | 13.35       |
| Section B          | 0.02                             | 268.57               | 01Jan2000, 11:56 | 13.35       |
| Section J          | 0.06                             | 668.18               | 01Jan2000, 11:56 | 11.31       |
| Reservoir B        | 0.02                             | 6.72                 | 01Jan2000, 11:50 | 6.55        |
| Reservoir H        | 0.01                             | 105.08               | 01Jan2000, 12:02 | 13.16       |
| Section I          | 0.02                             | 221.11               | 01Jan2000, 11:56 | 13.35       |
| Reservoir I        | 0.02                             | 120.18               | 01Jan2000, 12:02 | 13.12       |
| Reservoir J        | 0.12                             | 98.01                | 01Jan2000, 12:46 | 8.25        |
| Outfall            | 0.12                             | 98.01                | 01Jan2000, 12:46 | 8.25        |



# Subbasin: Section H

Area (ft<sup>2</sup>): 0.01

Downstream: Reservoir H

### Loss Rate: SCS

|                         |    |
|-------------------------|----|
| Percent Impervious Area | 0  |
| Curve Number            | 98 |

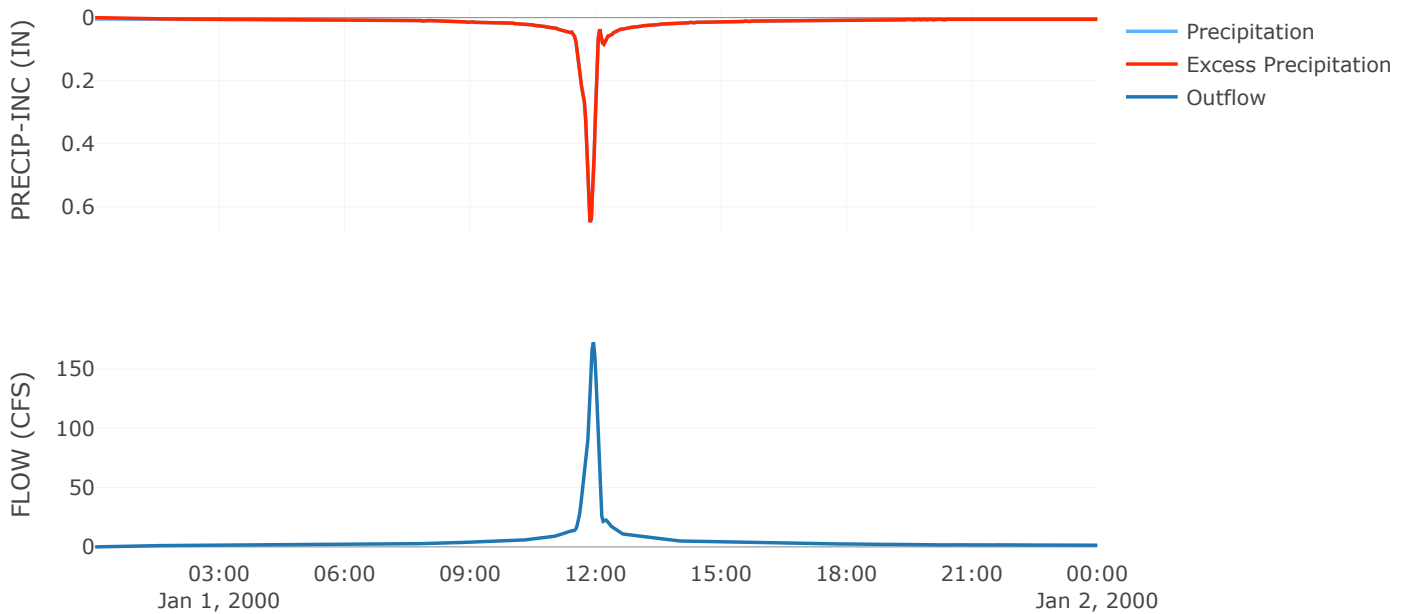
### Transform: SCS

|                |          |
|----------------|----------|
| Lag            | 3        |
| Unitgraph Type | Standard |

### Results: Section H

|                                |                  |
|--------------------------------|------------------|
| Peak Discharge (CFS)           | 172.49           |
| Time of Peak Discharge         | 01Jan2000, 11:56 |
| Volume (IN)                    | 13.35            |
| Precipitation Volume (AC - FT) | 10.81            |
| Loss Volume (AC - FT)          | 0.19             |
| Excess Volume (AC - FT)        | 10.62            |
| Direct Runoff Volume (AC - FT) | 10.61            |
| Baseflow Volume (AC - FT)      | 0                |

Precipitation and Outflow



# Subbasin: Section B

Area (ft<sup>2</sup>): 0.02

Downstream: Reservoir B

### Loss Rate: SCS

|                         |    |
|-------------------------|----|
| Percent Impervious Area | 0  |
| Curve Number            | 98 |

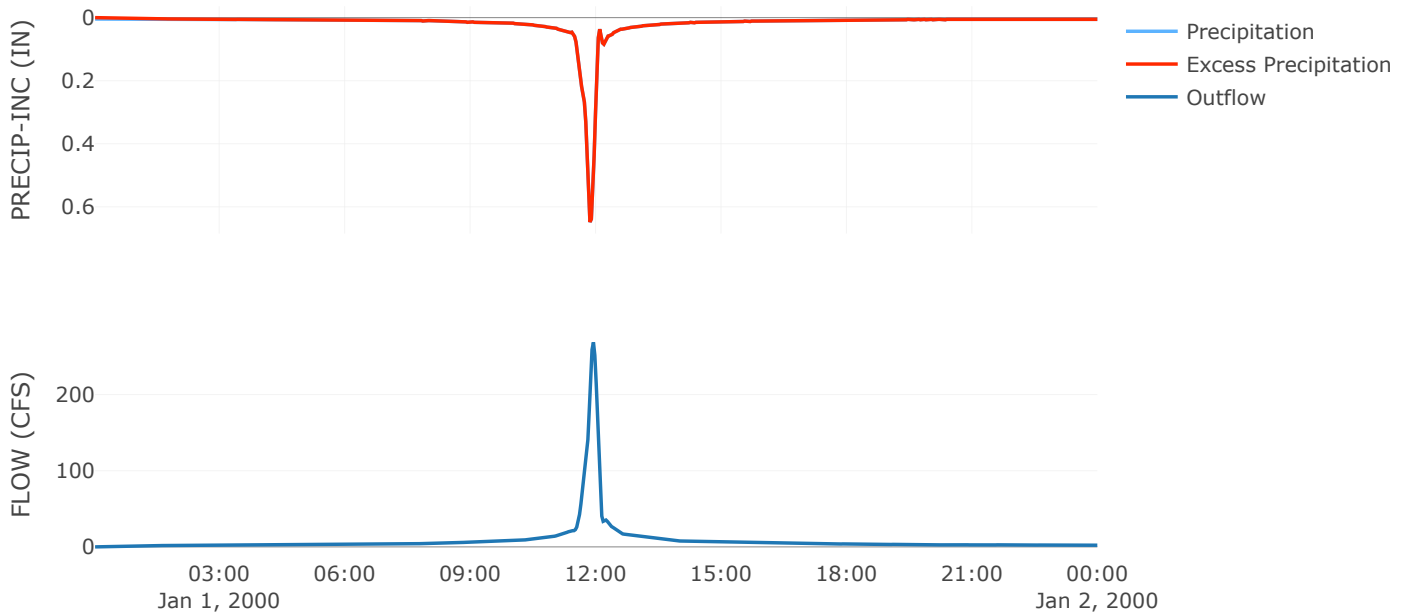
### Transform: SCS

|                |          |
|----------------|----------|
| Lag            | 3        |
| Unitgraph Type | Standard |

### Results: Section B

|                                |                  |
|--------------------------------|------------------|
| Peak Discharge (CFS)           | 268.57           |
| Time of Peak Discharge         | 01Jan2000, 11:56 |
| Volume (IN)                    | 13.35            |
| Precipitation Volume (AC - FT) | 16.83            |
| Loss Volume (AC - FT)          | 0.3              |
| Excess Volume (AC - FT)        | 16.53            |
| Direct Runoff Volume (AC - FT) | 16.52            |
| Baseflow Volume (AC - FT)      | 0                |

Precipitation and Outflow



# Subbasin: Section J

Area (ft<sup>2</sup>): 0.06

Downstream: Reservoir J

### Loss Rate: SCS

|                         |       |
|-------------------------|-------|
| Percent Impervious Area | 0     |
| Curve Number            | 82.31 |

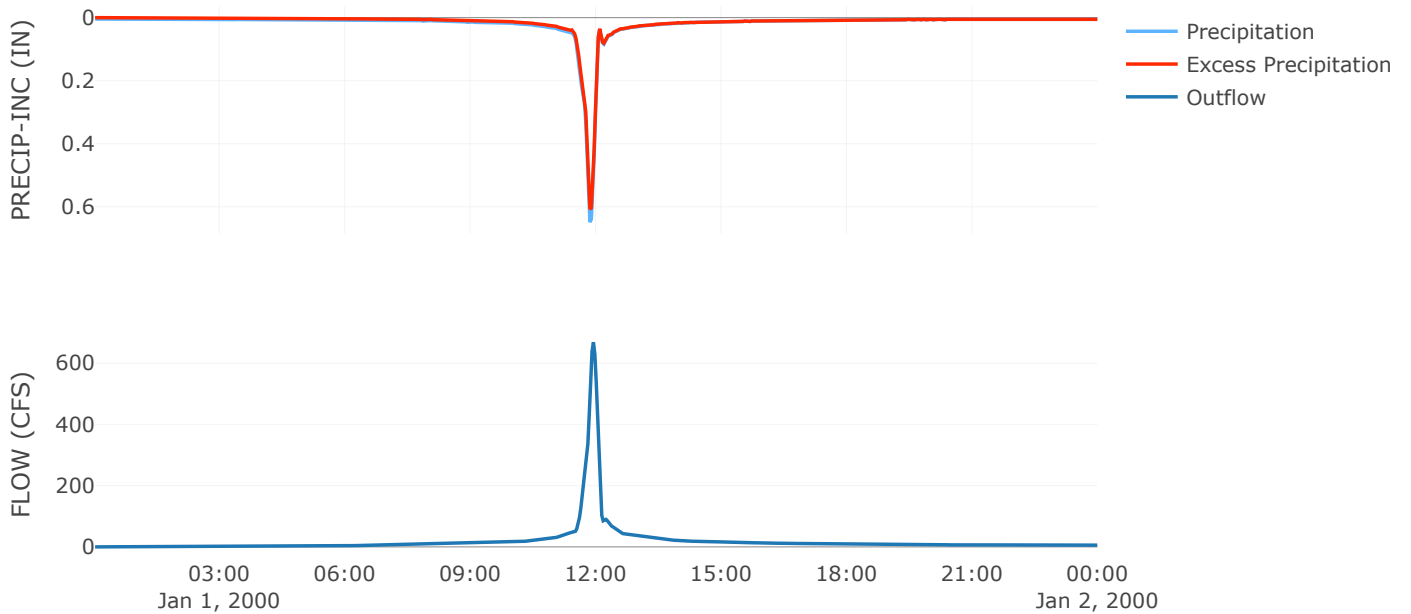
### Transform: SCS

|                |          |
|----------------|----------|
| Lag            | 3        |
| Unitgraph Type | Standard |

### Results: Section J

|                                |                  |
|--------------------------------|------------------|
| Peak Discharge (CFS)           | 668.18           |
| Time of Peak Discharge         | 01Jan2000, 11:56 |
| Volume (IN)                    | 11.31            |
| Precipitation Volume (AC - FT) | 44.54            |
| Loss Volume (AC - FT)          | 7.46             |
| Excess Volume (AC - FT)        | 37.08            |
| Direct Runoff Volume (AC - FT) | 37.04            |
| Baseflow Volume (AC - FT)      | 0                |

Precipitation and Outflow



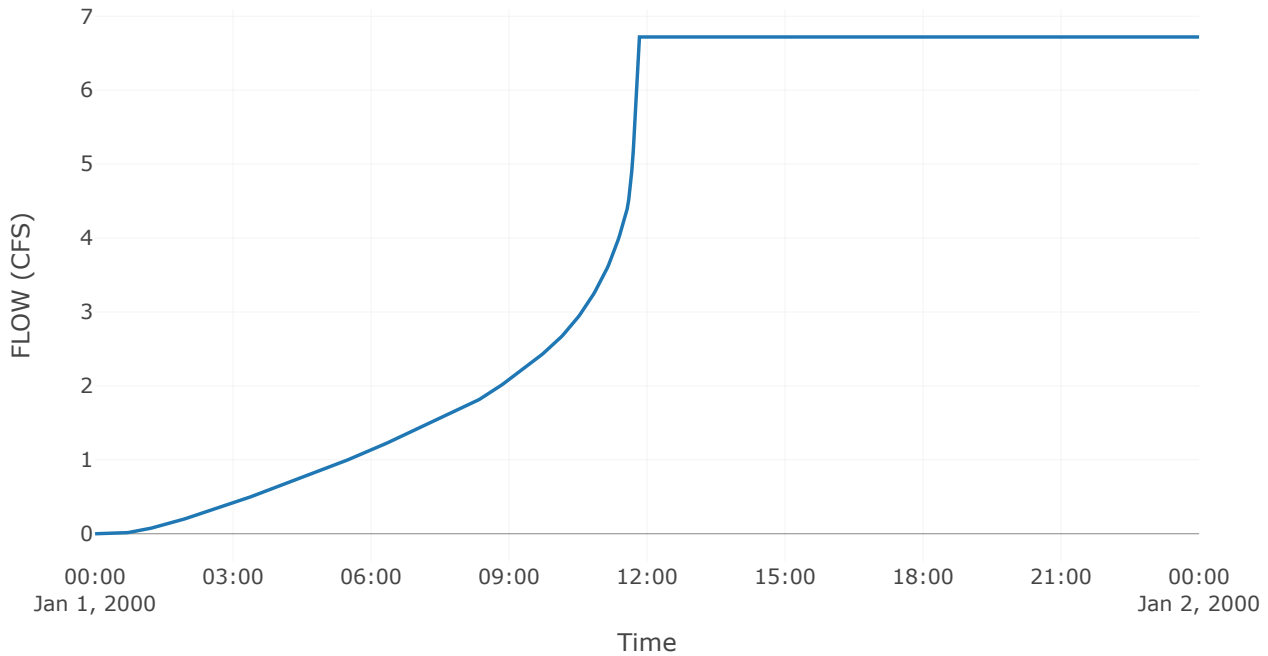
# Reservoir: Reservoir B

Downstream : Reservoir J

## Results: Reservoir B

|                            |                  |
|----------------------------|------------------|
| Peak Discharge (CFS)       | 6.72             |
| Time of Peak Discharge     | 01Jan2000, 11:50 |
| Volume (IN)                | 6.55             |
| Peak Inflow (CFS)          | 268.57           |
| Time of Peak Inflow        | 01Jan2000, 11:56 |
| Inflow Volume (AC - FT)    | 16.52            |
| Maximum Storage (AC - FT)  | 10.93            |
| Peak Elevation (FT)        | 954.43           |
| Discharge Volume (AC - FT) | 8.11             |

Outflow



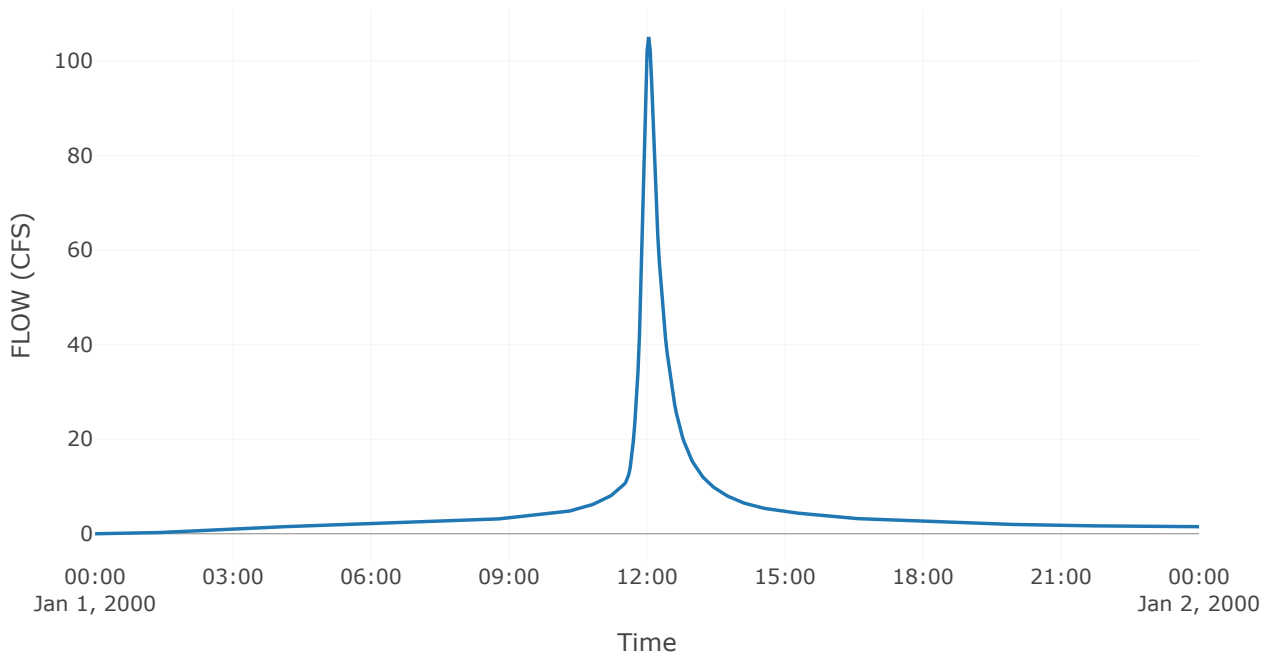
# Reservoir: Reservoir H

**Downstream** : Reservoir J

## Results: Reservoir H

|                            |                  |
|----------------------------|------------------|
| Peak Discharge (CFS)       | 105.08           |
| Time of Peak Discharge     | 01Jan2000, 12:02 |
| Volume (IN)                | 13.16            |
| Peak Inflow (CFS)          | 172.49           |
| Time of Peak Inflow        | 01Jan2000, 11:56 |
| Inflow Volume (AC - FT)    | 10.61            |
| Maximum Storage (AC - FT)  | 6.33             |
| Peak Elevation (FT)        | 947.43           |
| Discharge Volume (AC - FT) | 10.46            |

Outflow



# Subbasin: Section I

**Area (ft<sup>2</sup>)** : 0.02

**Downstream** : Reservoir I

### Loss Rate: SCS

|                         |    |
|-------------------------|----|
| Percent Impervious Area | 0  |
| Curve Number            | 98 |

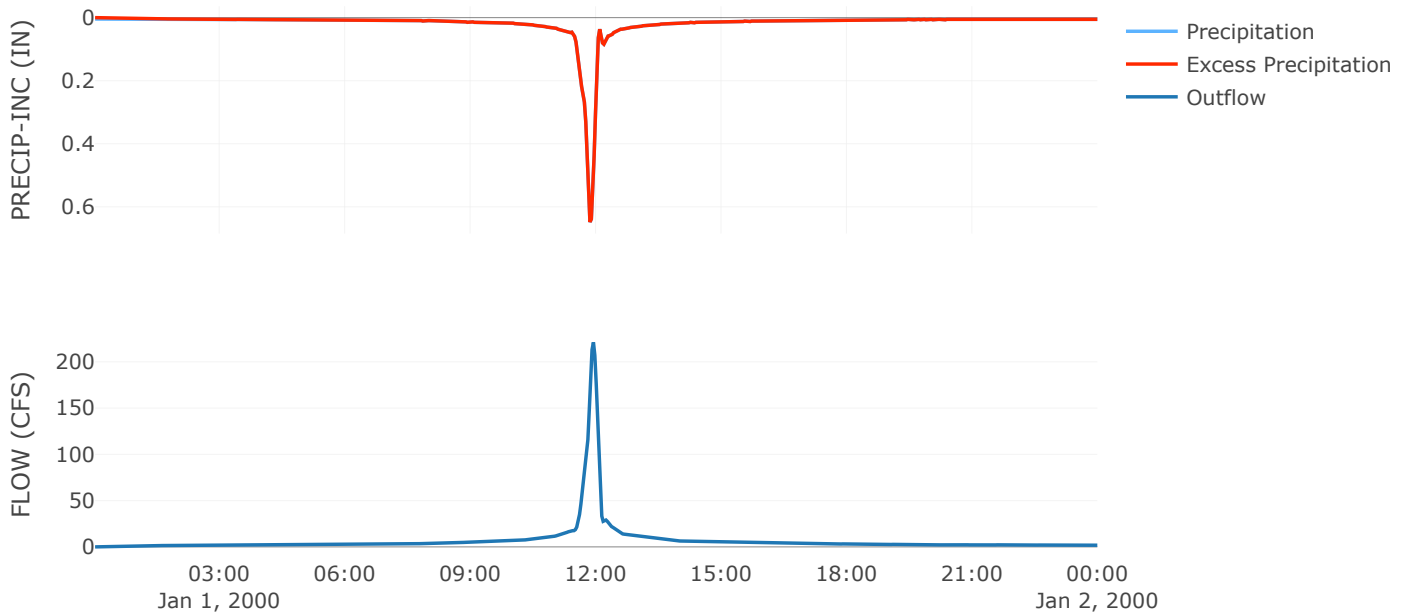
### Transform: SCS

|                |          |
|----------------|----------|
| Lag            | 3        |
| Unitgraph Type | Standard |

### Results: Section I

|                                |                  |
|--------------------------------|------------------|
| Peak Discharge (CFS)           | 221.11           |
| Time of Peak Discharge         | 01Jan2000, 11:56 |
| Volume (IN)                    | 13.35            |
| Precipitation Volume (AC - FT) | 13.85            |
| Loss Volume (AC - FT)          | 0.25             |
| Excess Volume (AC - FT)        | 13.61            |
| Direct Runoff Volume (AC - FT) | 13.6             |
| Baseflow Volume (AC - FT)      | 0                |

Precipitation and Outflow



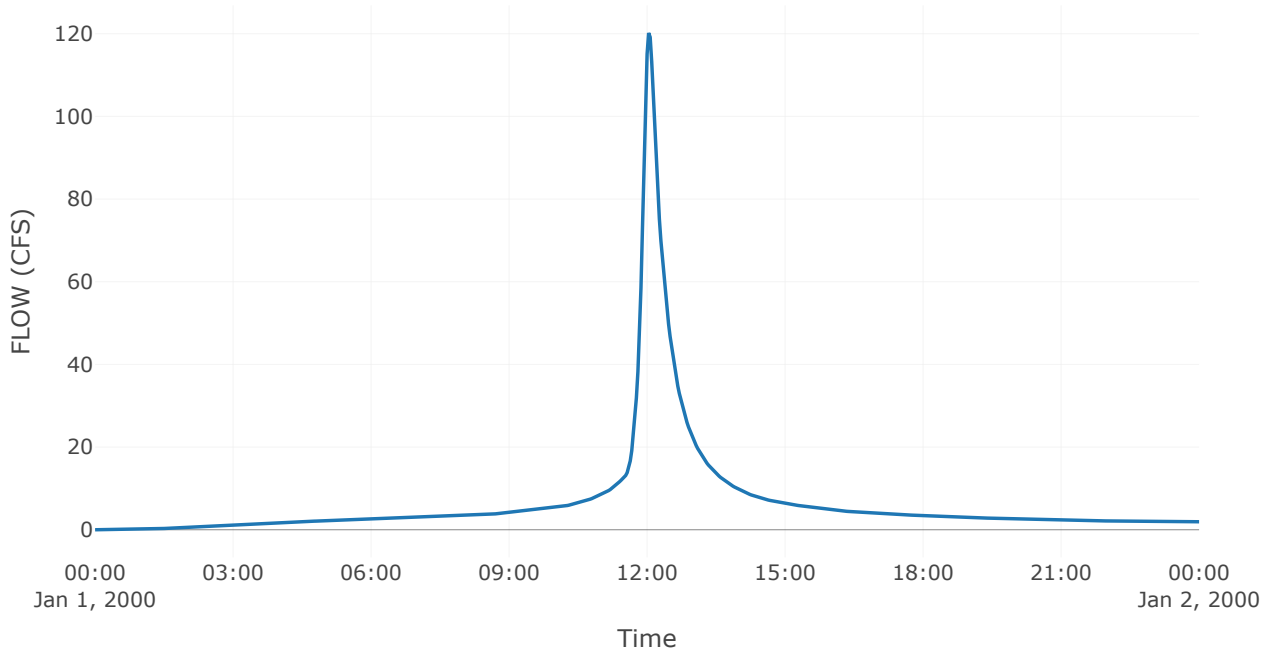
# Reservoir: Reservoir I

Downstream : Reservoir J

## Results: Reservoir I

|                            |                  |
|----------------------------|------------------|
| Peak Discharge (CFS)       | 120.18           |
| Time of Peak Discharge     | 01Jan2000, 12:02 |
| Volume (IN)                | 13.12            |
| Peak Inflow (CFS)          | 221.11           |
| Time of Peak Inflow        | 01Jan2000, 11:56 |
| Inflow Volume (AC - FT)    | 13.6             |
| Maximum Storage (AC - FT)  | 18.95            |
| Peak Elevation (FT)        | 946.47           |
| Discharge Volume (AC - FT) | 13.36            |

Outflow



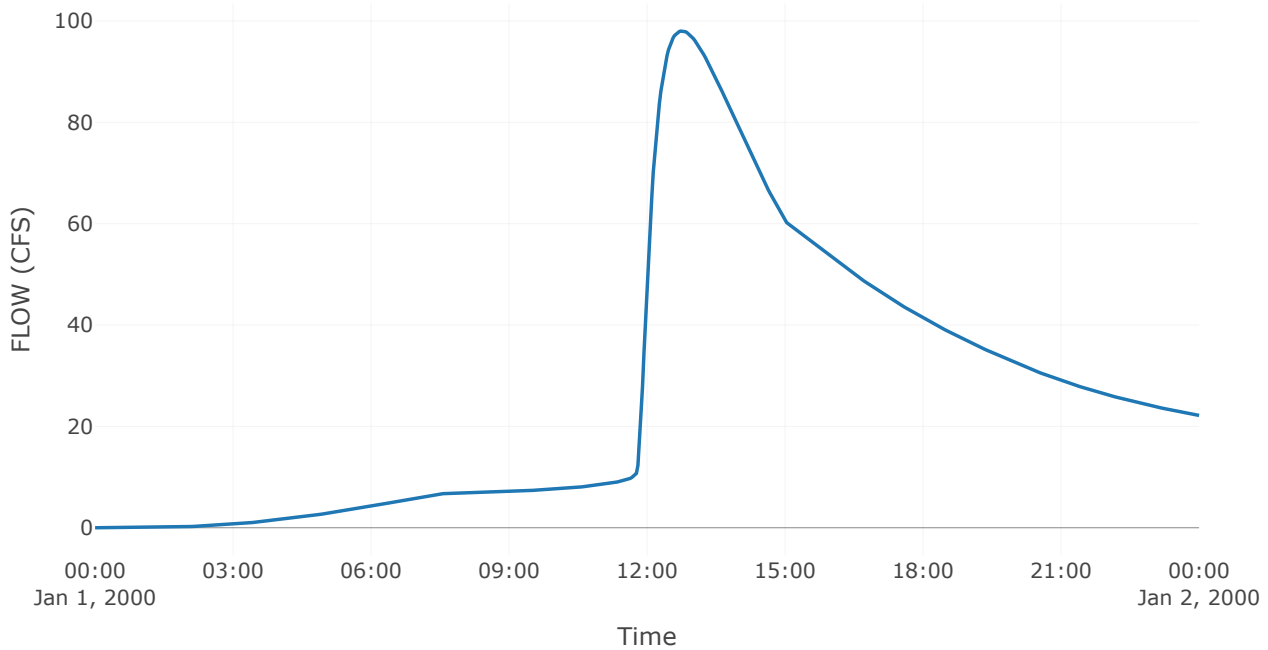
# Reservoir: Reservoir J

**Downstream** : Outfall

## Results: Reservoir J

|                            |                  |
|----------------------------|------------------|
| Peak Discharge (CFS)       | 98.01            |
| Time of Peak Discharge     | 01Jan2000, 12:46 |
| Volume (IN)                | 8.25             |
| Peak Inflow (CFS)          | 845.09           |
| Time of Peak Inflow        | 01Jan2000, 11:56 |
| Inflow Volume (AC - FT)    | 68.97            |
| Maximum Storage (AC - FT)  | 34.02            |
| Peak Elevation (FT)        | 931.31           |
| Discharge Volume (AC - FT) | 52.17            |

Outflow





# Sink: Outfall

## Results: Outfall

|                        |                  |
|------------------------|------------------|
| Peak Discharge (CFS)   | 98.01            |
| Time of Peak Discharge | 01Jan2000, 12:46 |
| Volume (IN)            | 8.25             |

